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A COMPUTATIONAL PROCEDURE FOR THE PROTECTION OF  
INDUSTRIAL POWER SYSTEMS(U) PENNSYLVANIA STATE UNIV  
UNIVERSITY PARK DEPT OF ELECTRICAL ENGINEERING

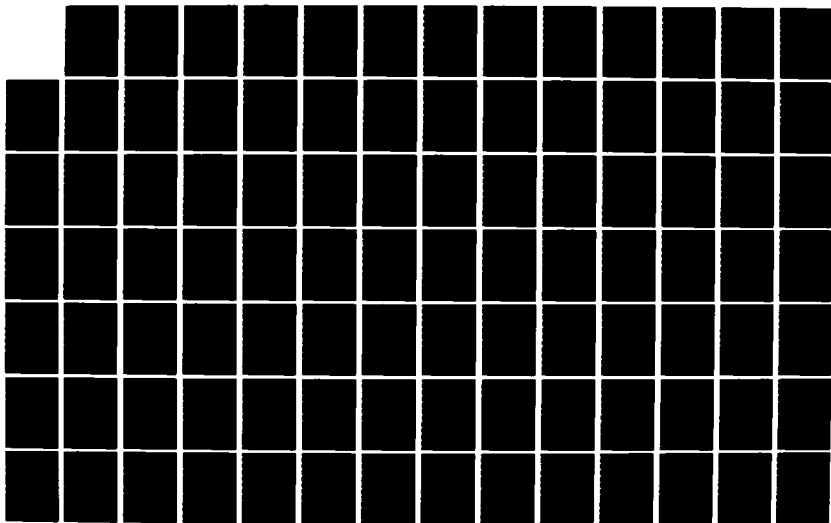
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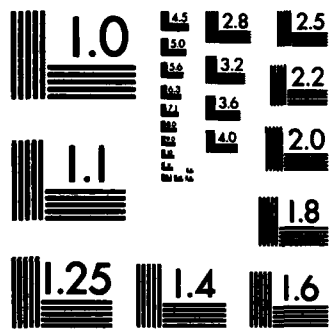
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The Pennsylvania State University  
The Graduate School  
Department of Electrical Engineering

A Computational Procedure for the Protection of  
Industrial Power Systems

A Thesis in  
Electrical Engineering

by

Charles N. Salmond

Submitted in Partial Fulfillment  
of the Requirements  
for the Degree of

Master of Science

November 1981

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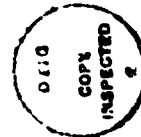
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## ABSTRACT

→ A procedure is presented that allows an engineer to coordinate protective devices consisting of fuses, circuit breakers, and over-current relays based upon load and fault currents. The resulting digital-computer program makes many of the decisions requiring very little prior in-depth knowledge of protective devices and power systems for its utilization.

The coordination procedure consists of six separate programs that must run in sequence, as the output from one program forms the input for the next program. This reduces in size of internal computer storage required.

The theory is presented with an explanation of each algorithm followed by a basic flow chart. An example computer run is presented at the end.



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## 1. INTRODUCTION

A prime objective of electrical engineers working on the design, operation, or maintenance of electrical power systems is to provide reliable, efficient power to their customers. The distribution system has always been a weak link in the power chain. Often, the catastrophic results of a fault are easily seen, but the cause may be extremely difficult to find. A distribution system, either in the utility or the user's facilities that is not adequately protected from electrical faults is both dangerous and costly. An unsatisfactorily protected system can cause considerable inconvenience and damage to equipment. Adequate protection is not a set definition. Each load system is different with its own set of boundary values.

In a distribution system, the flexibility of design reduces near the generator or the load. Usually the generator or load protection is designed as an integral part of the equipment by the manufacturer and any changes should only be undertaken with their counsel. Moving away from the generator or load, the priority shifts from load protection to distribution protection. It must never be forgotten that the load, distribution, and generation systems must be protected in such a way that a device that operates satisfactorily in one system cannot have a detrimental effect on another system. In this thesis the distribution section is attached from an infinite-bus power source to the load-protection device. The programs provide the

proper setting of a chosen device in order to provide good protective coordination. Proper coordination is achieved when a device closest to the fault clears the fault or overload condition before the rest of the system is disturbed. In order to achieve this end by manual means, extensive mathematical calculations and experience are required. As a direct result, proper coordination is often not achieved. The use of digital computers to solve the coordination problem makes a more exacting solution. However, computers with large internal memory are required to solve these problems. Several approaches to computer solutions have been published [1-4].

#### Problem Statement

The purpose of this thesis is to develop the procedure and an interactive computer program for a generalized case of device coordination. This coordination should include fuses, relays, and molded case circuit breakers. The phases of research are as follows.

1. Develop a computer procedure to compute the one-line program per unit values.
2. Develop a computer procedure to perform a load-flow analysis.
3. Develop a computer procedure to compute line-to-line ground and three-phase faults.
4. Develop and apply procedure for mathematical representation of line X/R data, fuse, molded-case circuit breaker, and relay-curve time-current characteristics.

5. Develop a computer procedure to coordinate the devices from phase 4 with the data derived from phases 2 and 3.

Although the coordination programs are written for the PDP10 computer, it requires no more than 25K bytes of internal memory and a disk unit to solve any system of 30 buses and 100 elements. Almost any large system can be reduced to its smaller parts composed of 30 buses or less. As each segment is coordinated, it can be represented by a load and its protective device. In this manner a 300-bus system could be divided into smaller segments and in 11 runs would be completely coordinated. The step-by-step approach used here allows for insertion or extraction of data before proceeding to the next step. Figure 1.1 is a basic flow chart of the coordination program. Hereafter it will be referred to by its individual parts.

When the coordination process has been completed, a load flow study and a fault analysis has been performed as well. The major assumptions that have been made are listed here. Other minor ones are included in the corresponding chapters. These assumptions have been made in an effort to keep the solution as general as possible.

1. The incoming line is assumed to be an infinite bus.
2. Assymetrical currents are neglected. Devices are coordinated on the basis of symmetrical fault currents.
3. Only synchronous-motor contributions to the fault currents are recognized. If a large induction motor

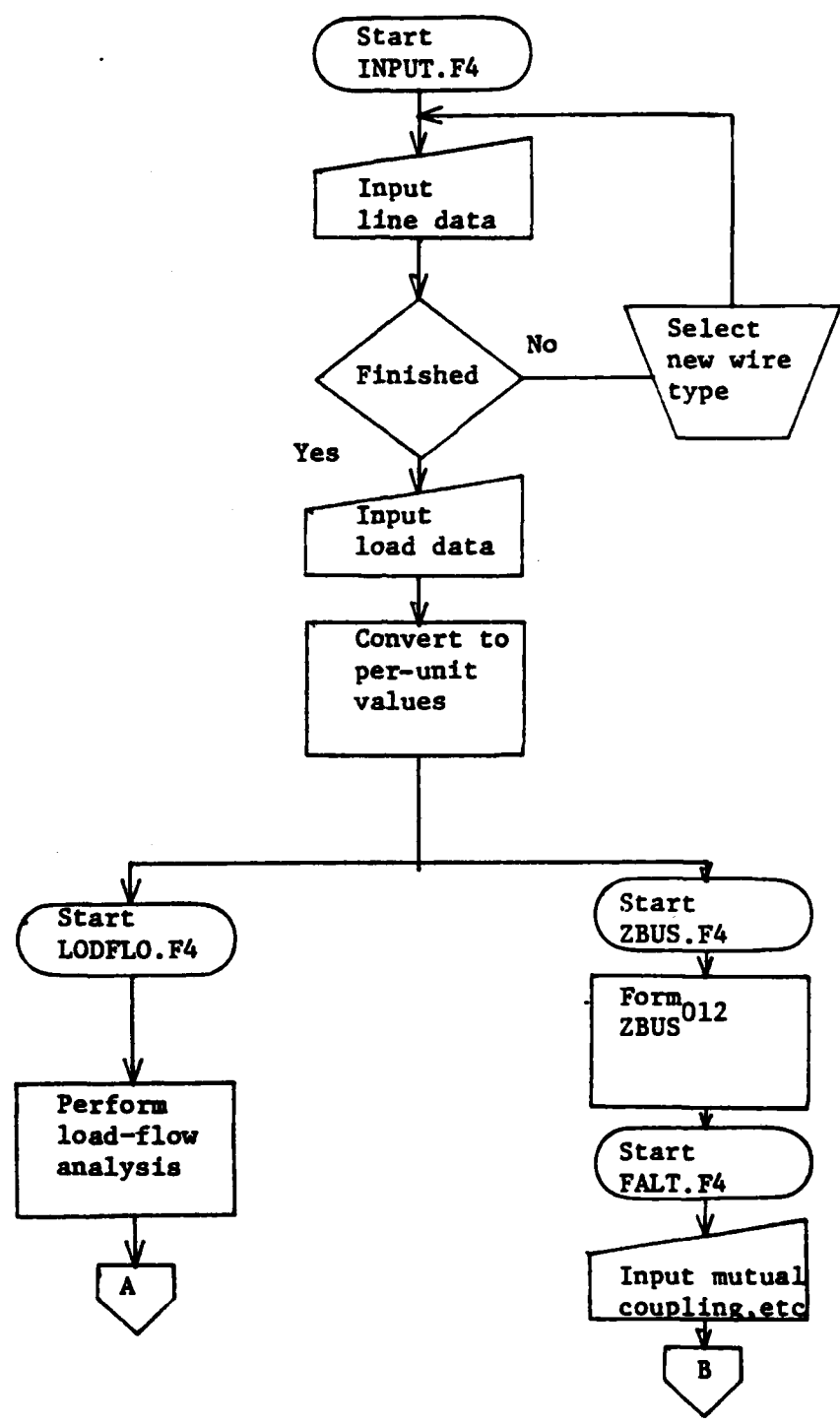


Figure 1.1. Flow chart of the coordination procedure.

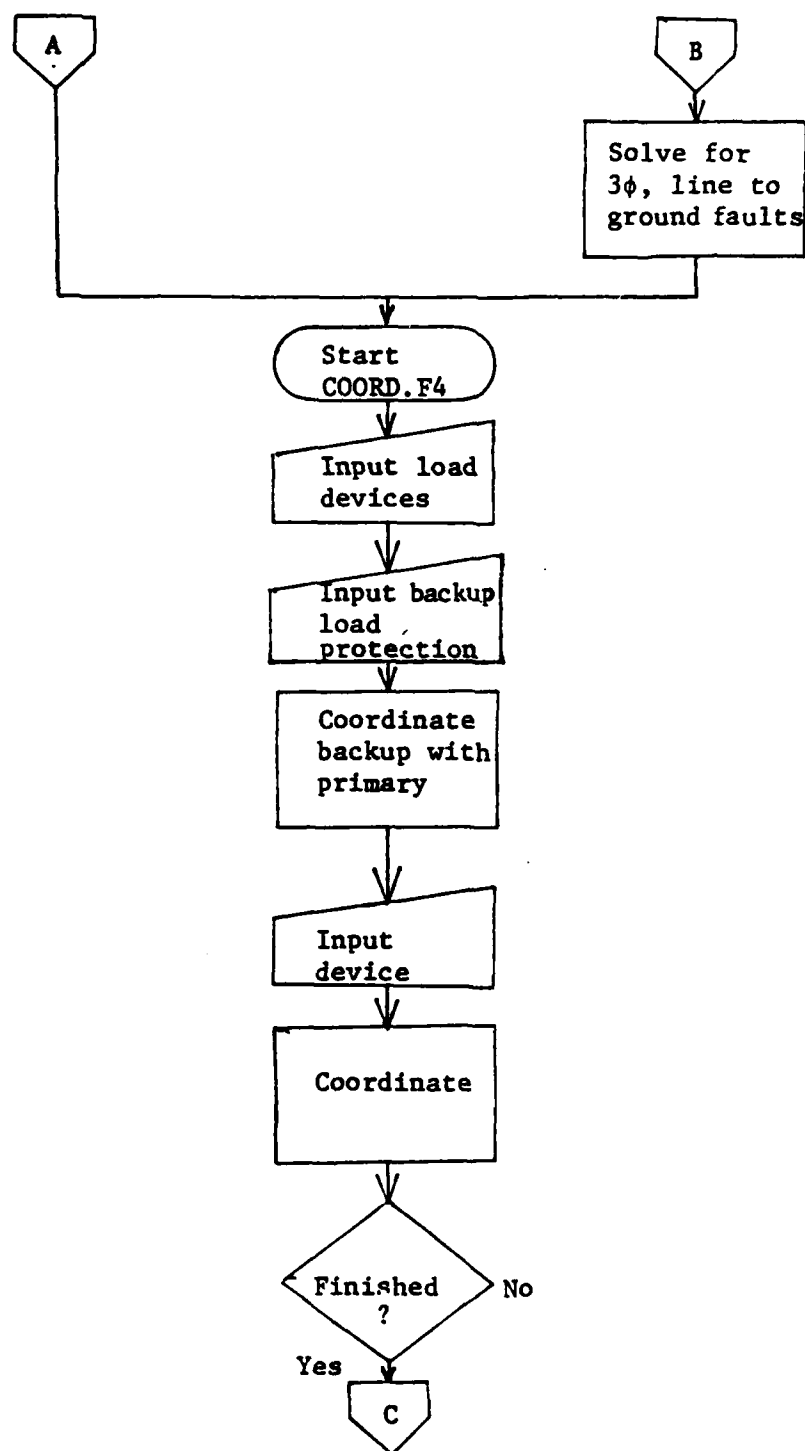


Figure 1.1. Continued.

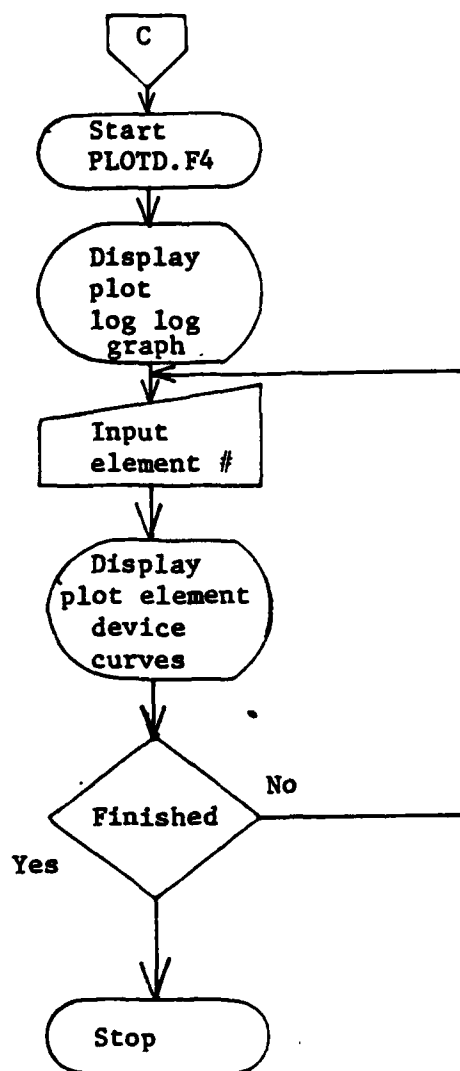


Figure 1.1. Continued.



is present, it may be added as a fictitious synchronous motor.

4. Line-charging shunt admittance is ignored.
5. Prefault current and voltages are neglected in fault-current computations.
6. Different sizes of fuses have the same time-current curve shape.
7. Overload conditions are 125% of full load.
8. The system has a balanced three-phase load.

In this thesis each phase of research in the problem statement has a chapter devoted to it. After describing the computational methods used in curve smoothing, the coordination problem begins with data input. Next the fault currents are solved followed by the actual coordination program and device response graphing. Finally, a sample distribution system coordination problem is described.

## 2. CURVE SMOOTHING AND DIGITIZING

### General

In this chapter, the methods for using a data digitizing "numonics" device and the curve smoothing program of Appendix A are explained. The various device equations that were found that adequately represented the particular device's time current curve are also described.

A method was described in Wagner [1] for performing this by using the PDP10 computer. This least-square curve-fitting program [1] was expanded to eliminate any external subroutines that may not be available. The coordination program makes extensive use of polynomial functions whose coefficients were derived by using the least-squares curve-smoothing technique.

### Curve Smoothing

Electrical Cables. Coefficients for the mathematical modeling of resistance and reactance were taken from data for mine power cable [5]. This is used as only one type of cable or wire. Any other type may be modeled by the same procedure. For instance, either actual cable or line data could be used directly [6], or the theoretical resistance and reactance for each size could be calculated [5-8].

Fuses. Two types of fuses are used in the coordination program. These are current-limiting and solid-material boric-acid power fuses. In each case, the curve shape is assumed to be the same for different sizes. The low-current asymptotic value is called the "offset." Each fuse has a minimum and a typical operating time. In fuse coordination, both values must be used in describing the operating envelope of a particular fuse. The higher typical operating time curve is referred to as "Offset 1." By this means, any fuse can be completely described by four equations, where:

$$\text{Log } T_{\min} = \left( \sum_{j=0}^n a_j (\text{Log Current-Offset})^j \right) - 2 \quad (2.1)$$

$$\text{Log } T_{yp} = \left( \sum_{k=0}^n a_k (\text{Log Current-Offset1})^k \right) - 2 \quad (2.2)$$

Fuses are selected also by using mathematical models. To select a fuse, the program uses the overload-current value as the variable in the polynomial function. The result is the device number. In curve smoothing, variables can assume no value less or greater than those originally used as data for the curve-smoothing program, or large errors can result.

Molded-Case Circuit Breakers. Like the fuses discussed above, each molded-case circuit breaker consists of an operating envelope bounded by a minimum value and a maximum value. Unlike fuses, however,

a table look-up approach is used in selection of a device and its setting because of the smaller number of sizes and magnetic-trip settings.

Relays. Wagner [1] discusses the representation of the family of relay curves for each type with one polynomial equation comprised of four coefficients. The 0<sup>th</sup> power coefficient was left out as a variable for coordination. Unfortunately, this method proves unsatisfactory when working with more than one relay type. It was found that each relay could be represented by five coefficients. The 0<sup>th</sup> power coefficient is necessary in that it provides the time displacement necessary for minimum time dial setting. The curves were derived using the procedure below.

Westinghouse Company type relays were used. An average curve was taken as time-dial 4. This curve was reduced to a polynomial function. The time difference between time-dial 4 and time-dial 1/2 taken at 20 times the pickup value is subtracted from the 0<sup>th</sup> coefficient. Twenty times pickup was a good value for computing the time difference as the time value changes very little for increases in current beyond that point. The resultant curve was the average shape of a time-dial setting of 4 now shifted to minimum setting. This allows for time values computed during coordination to be summed with the 0<sup>th</sup> coefficient. The curves are then represented as follows:

$$\text{Log Time} = \left( \sum_{j=0}^n a_j (\log(\text{Current Value}))^j \right) +$$

Log (Time Setting)

This allows the use of more than one type of relay in each coordination as it separates time setting value from relay type.

Curve Digitizing. The device's time versus current curves were digitized by using a NUMONICS electronic graphics calculator (EGC). The NUMONICS EGC is designed to translate graphic information on any medium into digital information. Complete information on its usage may be found in -NUMONICS Electronic Graphics Calculator [9]. The NUMONICS EGC then provided a convenient way to enter X-Y coordinate data representing any curve onto disk. Since this device works in length in inches, the data has to be normalized to its proper units.

A simple program DIGIT.F4 was written to normalize and store onto disk the NUMONICS EGC information. The program flow chart is shown in Figure 2.1.

Curve Smoothing. The curve-smoothing program contained in Wagner [1] was used as a basis for the curve smoothing program DEV.F4. Unnecessary parts were removed and a double precision matrix inversion routine was added. This prevented the necessity of using subroutines contained in the computer's SSP routine files. The inversion routine was converted from The Pennsylvania State University Computer Center's matrix inversion routine CMINV which inverts a complex square matrix. This routine in turn was converted from the SSP routine MINV [10].

Since it has its own inversion routine, this curve smoothing program can be easily expanded to any number of points and any dimension of fit by changing the dimension statements. The flow chart and procedure remains the same as in [1]. A complete program listing may be found in Appendix A.

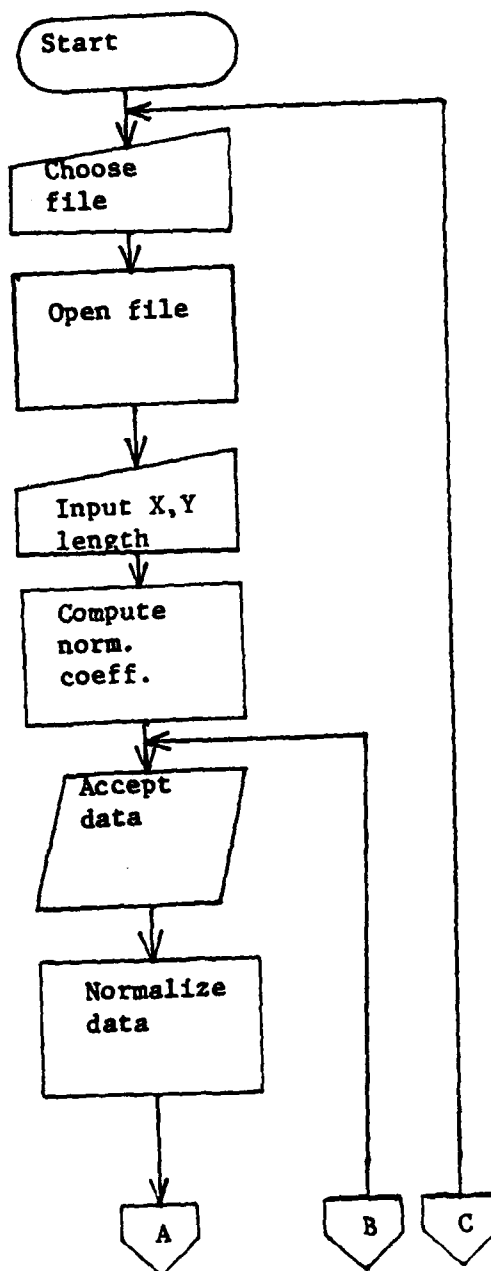


Figure 2.1. Curve-digitizing flow chart.

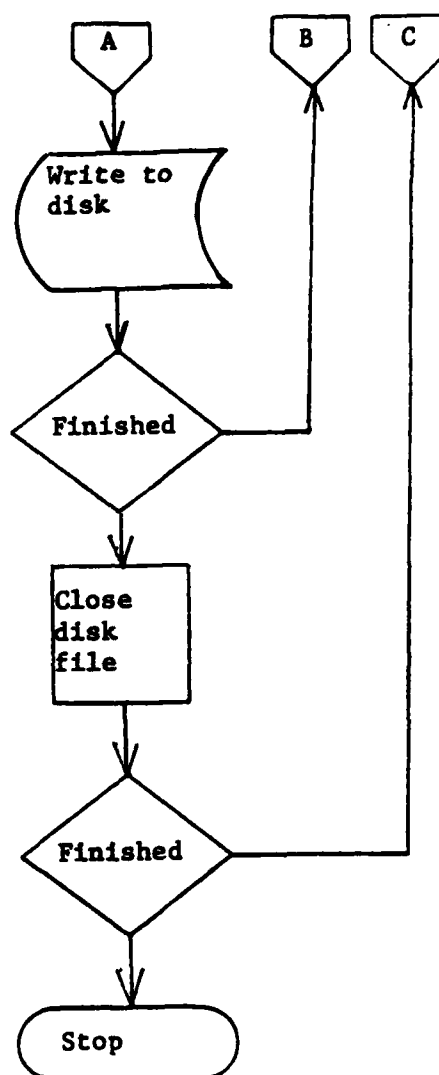


Figure 2.1. Continued.

### Summary

Polynomial functions describe the various device-response curves, line X/R data, and fuse-selection criteria. The coefficients for these polynomial functions are found from data entered using a digital-data device or manual input. This data is reduced by a curve-smoothing program to the desired function.

The start of the coordination problem begins in the next chapter with line and load data entry.



### 3. THE INPUT OF DISTRIBUTION-SYSTEM DATA

#### General

Usually, the first step in performing any calculations on a distribution system is to reduce all system values to per unit. The methods used to do this in the program will be described in this chapter. Errors can be introduced easily when converting to the per unit system using manual calculations. Program INPUT.F4 was written to perform this function as well as computing line resistance and reactance values and storing all system data on disk for use in subsequent programs.

#### Per-Unit Reduction

The program uses the following formulas to convert to the per-unit system [8]. (See Table 3.1 for variable definitions used in this thesis.)

$$Z_{\text{Base}} = (KV_{\text{Base}})^2 / MVA_{\text{Base}}$$

$$Z_{\text{P.U.}} = Z(\Omega) / Z_{\text{Base}}$$

$$I_{\text{Base}} = KVA_{\text{Base}} / KV_{\text{Base}}$$

Table 3.1. Variable definitions.

---

|                   |   |
|-------------------|---|
| $Z(\Omega)$       | element impedance                                 |
| $Z_{p.u.}$        | impedance in per unit                             |
| $X_d$             | subtransient reactance                            |
| $P_p$             | real power bus p                                  |
| $Q_p$             | reactive power bus p                              |
| $E_p$             | complex voltage bus p                             |
| $I_p$             | complex current bus p                             |
| $Y_{pq}$          | Y bus element bus p to q                          |
| $\bar{y}_{pq,rs}$ | admittance value from primitive admittance matrix |
| $Z_{pq}$          | Z bus element bus p to q                          |
| $z_{pq,pq}$       | impedance value from primitive impedance matrix   |
| $z_f$             | fault impedance                                   |
| $y_f$             | fault admittance                                  |

---

$$Z_{P.U.new} = Z_{P.U.given} \left( \frac{KV_{Base\ given}}{KV_{Base\ new}} \right)^2 \left( \frac{KVA_{Base\ new}}{KVA_{Base\ given}} \right)$$

Utilizing the above formulas it is possible then to represent all elements in the distribution system on a per-unit basis. Loads need to be included also in the one-line representation.

The program allows loads to be represented either by induction motor horsepower, synchronous motor horsepower, kVA, or current.

Loads are entered in the following format: Bus number/horsepower, kVA, current/power factor. The program assumes 100% efficiency so one must use:

$$HP_{Entered} = HP/Efficiency \quad (3.1)$$

If information on efficiency and power factors are unknown, the following equations may be used instead of 3.1 [9].

For induction motors, use:

$$HP_{Entered} = HP \times 1.1627$$

$$Power\ Factor = .86 \quad (3.2)$$

For synchronous motors use:

$$Unity\ Power\ Factor\ HP = 1.139 \times Horsepower \quad (3.5)$$

$$.8\ Power\ Factor\ HP = 1.18 \times Horsepower \quad (3.6)$$

### Formulae for Line Resistance and Reactance

Element data is entered in the following format: line bus/  
load bus/cable length in feet/wire size/transformer P.U. impedance/  
size in MVA/line voltage in KV/load voltage in KV.

Wire sizes that are entered in American wire gauge (AWG) are  
converted to MCM wire gauge by using the following formula [1]:

$$\text{MCM} = [(.005) \{(1.229)^{(36 \text{ AWG})^2}\}] \times 1000 \quad (3.7)$$

Once the wire size is in MCM, the line resistance and reactance are  
computed using the polynomial coefficients that were found by the  
procedure in Chapter 2.

$$\text{Resistance or reactance} = \sum_{j=0}^n a_j [\log(\text{MCM})]^j \quad (3.8)$$

The program should not be limited to just one wire type. The program  
does this by reading wire coefficients  $a_j$  above from disk so that each  
time the program is run it can compute element data using different wire  
types until the entire system has been completely entered.

Transformers become very important in that they can become the  
highest source of resistance and reactance. By their connections and  
neutral impedance, they determine the magnitude of zero-sequence current  
that will flow in the particular element. The program allows for this  
input and writes this information in the particular disk files for use  
later on in fault analysis.

Transformer inrush and withstand values must also be calculated. These values must be used in coordinating protective devices. These devices must pass inrush currents but open under conditions of exceeded transformer withstand currents. The algorithm in the program is based on average values. If test data is available this should be entered directly by changing the transformer data disk file directly after the program is run and before proceeding with coordinations. Inrush and withstand values are computed as follows [11]:

$$\text{Inrush} = 12 \times (\text{Transformer Base Current}) \quad (3.9)$$

$$\text{Withstand @2 Sec} = 25 \times (\text{Transformer Base Current}) \quad (3.10)$$

$$\text{Withstand @5 Sec} = 14.5 \times (\text{Transformer Base Current}) \quad (3.11)$$

Transformer withstand is some value between the two second value to the five second value and depends upon the transformer impedance. It is fairly easy, however, to have the device protect the complete range of withstand values and the program is written to accomplish this task.

Synchronous subtransient reactance is computed as follows [11]:

$$(\text{Per unit KVA}) \times (.17) = jX_d \quad (3.12)$$

One of the problems encountered in computing transmission line impedance is a reasonable calculation of the zero-sequence impedance. The computer program assumes that this value is two times the positive-sequence impedance [8] if nothing is entered when the computer asks for the zero-sequence impedance multiple. If a different value is entered, the computer multiplies the positive sequence reactive value by this multiple to arrive at the zero-sequence value.

A basic flow chart follows in Figure 3.1 with a complete program listing in Appendix B.

### Summary

The first step toward solving the coordination problem is completed. All element data has been converted to the per-unit representation. The next logical step is to perform a load-flow analysis to determine the full load currents in each element.

## Flow Chart Input

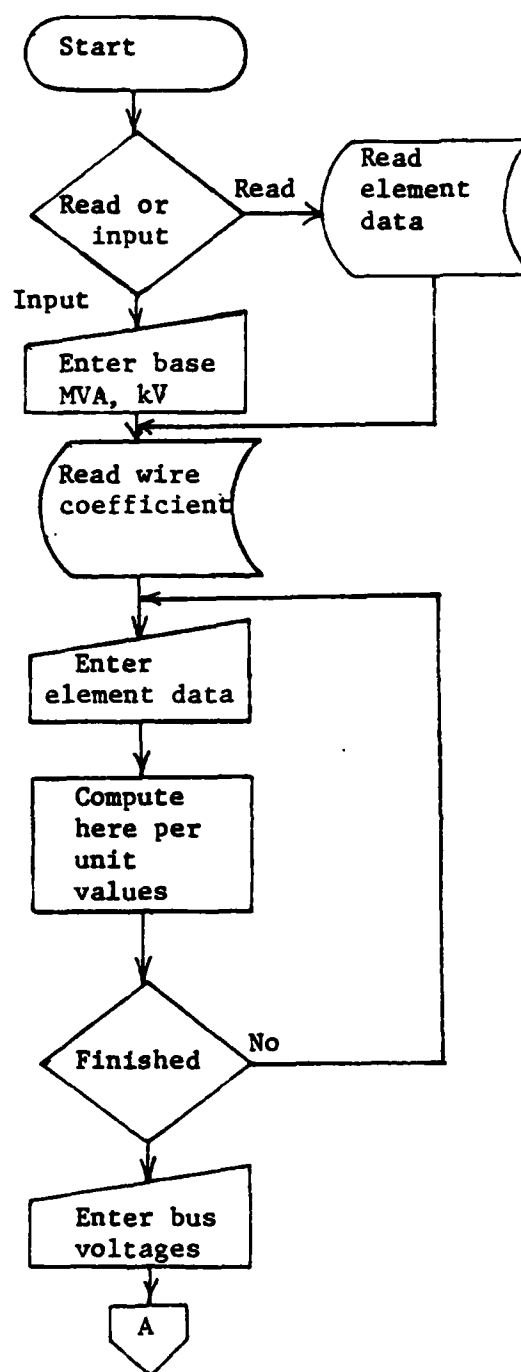


Figure 3.1. Per-unit calculations flow chart.

Input

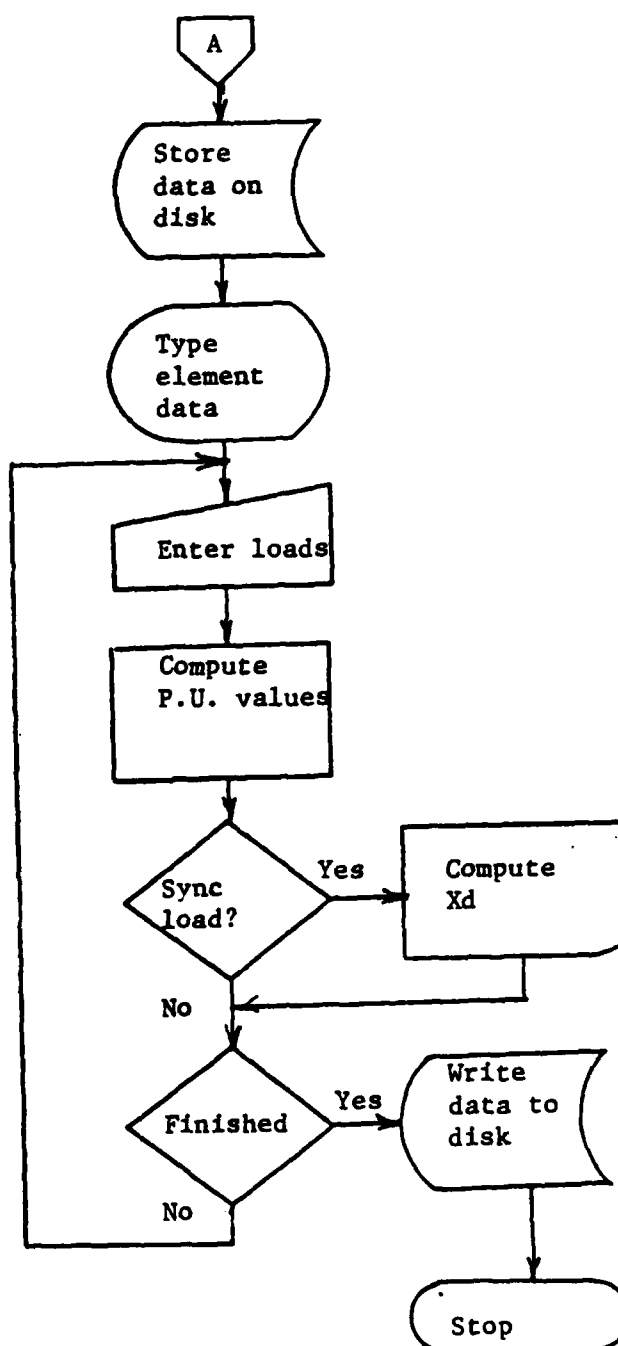


Figure 3.1. Continued.



#### 4. LOAD-FLOW ANALYSIS

##### General

In order to establish overload conditions on each element, the load currents must be determined. This is done by using a load flow analysis. The Newton-Raphson Method using Y-bus [12] was chosen because it required the least amount of iterations to obtain a solution to the load-flow problem.

##### Load Flow

In this method Y-bus must first be formed from the primitive-impedance network. When mutual coupling is ignored, Y-bus can be formed easily by algorithm. Any system can be completely represented by a set of equations [8,12].

$$I^{bus} = (Y^{bus})(E^{bus}) \quad (4.1)$$

$E^{bus}$  and  $I^{bus}$  are column matrices with one entry for each bus in the system.  $Y^{bus}$  is a square matrix of order equal to the number of buses in the system. Therefore, once all bus voltages are known and Y-bus is formed, matrix multiplication gives the desired load currents.

However, there is no direct approach to obtain the bus voltages. The only approach to use is that of iteration. The Newton-Raphson method accelerates the iteration process so that normally an accurate answer is obtained after three iterations.

The power at bus  $p$  is (from 4.1):

$$P_p - jQ_p = E_p^* I_p$$

$$P_p - jQ_p = E_p^* \sum_{q=1}^n Y_{pq} E_q \quad (4.2)$$

$$E_p = e_p + jf_p \sum_{q=1}^n Y_{pq} E_q = G_{pq} - jB_{pq} \quad (4.3)$$

So

$$P_p = \sum_{q=1}^n \{e_p (e_q G_{pq} + f_q B_{pq}) + (f_q G_{pq} - e_q B_{pq})\} \quad (4.4)$$

$$Q_p = \sum_{q=1}^n \{f_p (e_q G_{pq} + f_q B_{pq}) - e_p (f_q G_{pq} - e_q B_{pq})\} \quad (4.5)$$

The Newton-Raphson method uses the Jacobian matrix of partial-differential equations as follows:

$$\begin{bmatrix} \Delta P_1 \\ \Delta P_{n-1} \\ \vdots \\ \Delta Q_1 \\ \Delta Q_{n-1} \end{bmatrix} = \begin{bmatrix} \frac{\partial P_1}{\partial e_1} & \cdots & \frac{\partial P_1}{\partial e_{n-1}} & | & \frac{\partial P_1}{\partial f_1} & \cdots & \frac{\partial P_1}{\partial f_{n-1}} \\ \frac{\partial P_{n-1}}{\partial e_1} & \cdots & \frac{\partial P_{n-1}}{\partial e_{n-1}} & | & \frac{\partial P_{n-1}}{\partial f_1} & \cdots & \frac{\partial P_{n-1}}{\partial f_{n-1}} \\ \vdots & & \vdots & & \vdots & & \vdots \\ \frac{\partial Q_1}{\partial e_1} & \cdots & \frac{\partial Q_1}{\partial e_{n-1}} & | & \frac{\partial Q_1}{\partial f_1} & \cdots & \frac{\partial Q_1}{\partial f_{n-1}} \\ \frac{\partial Q_{n-1}}{\partial e_1} & \cdots & \frac{\partial Q_{n-1}}{\partial e_{n-1}} & | & \frac{\partial Q_{n-1}}{\partial f_1} & \cdots & \frac{\partial Q_{n-1}}{\partial f_{n-1}} \end{bmatrix} \begin{bmatrix} \Delta e_1 \\ \Delta e_{n-1} \\ \vdots \\ \Delta f_1 \\ \Delta f_{n-1} \end{bmatrix}$$

$$\begin{bmatrix} \Delta P \\ \Delta Q \end{bmatrix} = \begin{bmatrix} J_1 & | & J_2 \\ J_3 & | & J_4 \end{bmatrix} \begin{bmatrix} \Delta e \\ \Delta f \end{bmatrix} \quad (4.6)$$

The elements of the Jacobian matrix are found from the following equations:

$$J_1: \frac{\partial P}{\partial e_q} = e_p G_{pq} - f_p B_{pq} \quad q \neq p$$

$$\frac{\partial P}{\partial e_p} = 2e_p G_{pp} + f_p B_{pp} - f_p B_{pp} + \sum_{\substack{q=1 \\ q \neq p}}^n (e_q G_{pq} + f_q B_{pq}) \quad (4.7)$$

$$J_2: \frac{\partial P_p}{\partial f_q} = e_p B_{pq} + f_p G_{pq} \quad q \neq p$$

$$\frac{\partial P_p}{\partial f_p} = e_p B_{pp} + Z_{fp} G_{pp} - e_p B_{pp} + \sum_{\substack{q=1 \\ q \neq p}}^n (f_q G_{pq} - e_q B_{pq}) \quad (4.8)$$

$$J_3: \frac{\partial Q_p}{\partial e_q} = e_p B_{pq} + f_p G_{pq} \quad q \neq p$$

$$\frac{\partial Q_p}{\partial e_p} = f_p G_{pp} - f_p G_{pp} + Z_{ep} B_{pp} - \sum_{\substack{q=1 \\ q \neq p}}^n (f_q G_{pq} - e_q B_{pq}) \quad (4.9)$$

$$J_4: \frac{\partial Q_p}{\partial f_q} = e_p G_{pq} + f_p B_{pq} \quad q \neq p$$

$$\frac{\partial Q_p}{\partial f_p} = e_p G_{pp} + Z_{fp} B_{pp} - e_p G_{pp} + \sum_{\substack{q=1 \\ p \neq q}}^n (e_q G_{pq} + f_q B_{pq}) \quad (4.10)$$

Bus #1 or the swing-bus voltage is known. The swing bus is the bus that will provide whatever power the system requires. The program begins by forming Y-bus by using the primitive-impedance matrix generated by INPUT.F4 of Chapter 3. Since mutual coupling is ignored, the y-admittance matrix can be found by inverting each member of the z-impedance matrix found in disk file TEST.DAT.  $Y^{bus}$  matrix is formed using the algorithm below.

Diagonal elements are formed as the sum of all admittances connected to that bus or node. Off-diagonal elements are the negative of the admittance connected between the buses or nodes.

If more than 10 iterations are performed, the program stops and informs the user that either an error has been made in design or data entry. Upon successful completion of the program, a load-flow analysis may be obtained by printing file DISK.DAT. The program puts the load currents in the proper format and file for later use in the coordination program. A flow chart follows in Figure 4.1, and a complete listing is given in Appendix B.

### Summary

This load-flow analysis obtained can be very useful in analyzing the distribution-system design. It can be used to point out locations for power factor correction as well as potential problems due to undersized wiring.

The load currents found here are stored on disk to be used in the coordination program. The next step before beginning the

coordination program is to solve for all fault currents. Z-bus must be formed to compute these currents. The methods used to do this follows in the next chapter.

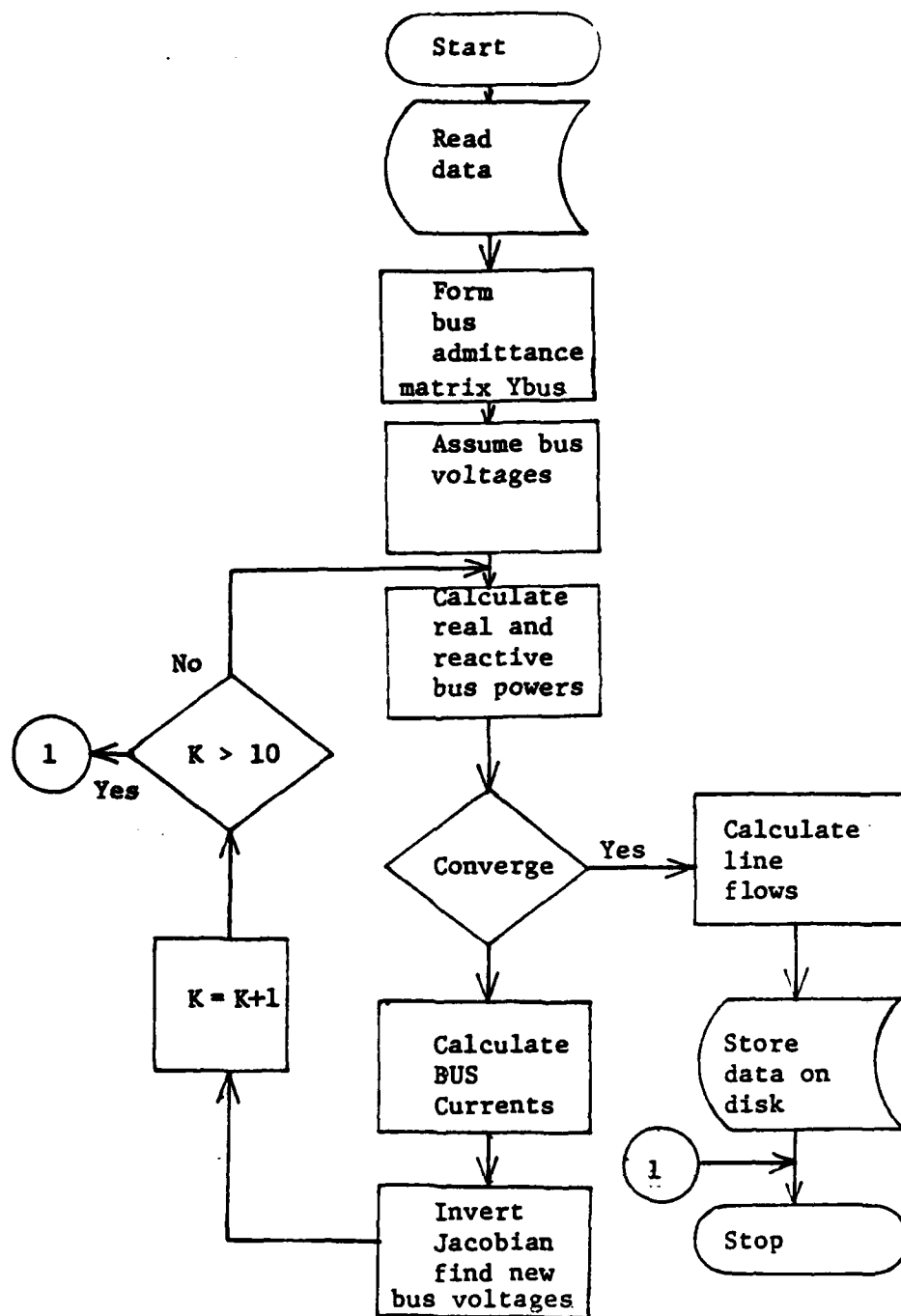


Figure 4.1. Newton-Raphson load-flow chart.

## 5. FORMATION OF IMPEDANCE-BUS NETWORK

### General

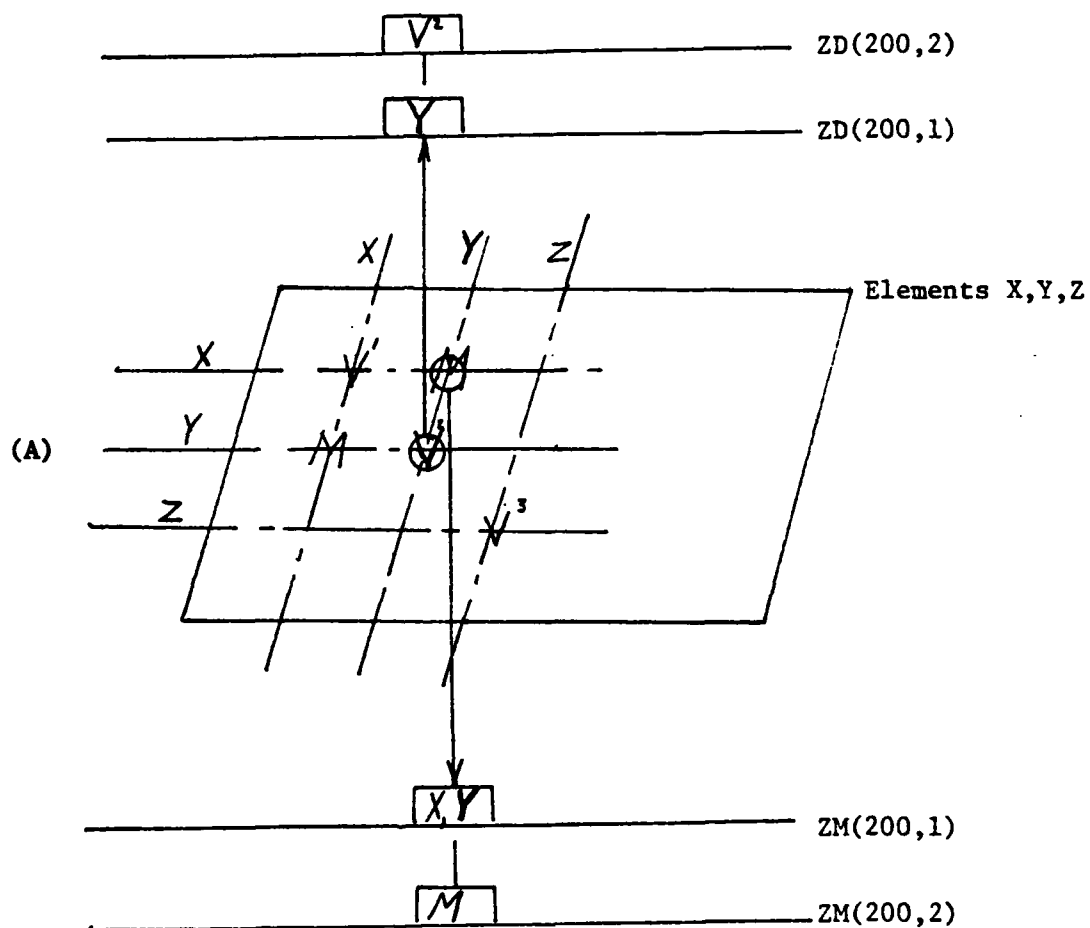
The formation of the impedance bus network ( $Z\text{-Bus}^{012}$ ) by algorithm is the first step toward solving for fault currents. In this chapter this algorithm will be discussed as well as other problems encountered in matrix compression.

### Formation of Z-Bus

Once the one line diagram has been completed, the primitive impedance matrix that was found in INPUT.F4 is a partially filled matrix. However, it is not in the proper format for the formation of Z-bus as it contains no coupling. The primitive impedance matrix must change from one of order equal to the number of buses to one of order equal to the number of elements. This matrix becomes a very large sparse matrix. The memory required to store this matrix becomes too large to fit in a small computer. A method was derived to only store the non zero values and their location in the matrix. Since the matrix is triangular only the top half is stored (Figure 5.1).

Diagonal elements found in INPUT.F4 are stored in "ZD." ZD is a three-dimensional matrix, ZD(200,2) where (X,1) is the element number and (X,2) is the diagonal value.





Number locations matrix (A) = (# elements)<sup>2</sup> X 2  
 Number of locations of alternate method = 8 X (# elements)

Figure 5.1. Transformation of square sparse primitive impedance.

The off diagonal mutual coupling  $Z_m$  is a three dimensional matrix also where  $(X,1)$  is the location value  $A+jB$ . Element A is coupled to element B. Location  $(X,2)$  is the coupling value. Fortunately, partitioning makes it necessary to assemble a square matrix for inversion of only the coupled elements. Since coupling only exists in zero sequence, this applies only to the zero-sequence Z-bus matrix.

In the formation of the Z-bus matrix, bus 1 is the reference bus for all calculations. Z-bus is formed by starting with element one and proceeding with each element in turn. An element is either a link or branch. A link means that both buses have been used earlier; a branch means they have not been used earlier.

Like Y-bus in Chapter 4 any system can be represented by

$$E_{bus}^{012} = Z_{bus}^{012} I_{bus}^{012}$$

Formation of  $Z_{bus}^{012}$  can be formed either by the incidence, network-matrices method [12] or by algorithm. Formation by algorithm is much simpler and is used here.

After forming the primitive impedance network, it is a straightforward application of the equations of Table 5.1.

Table 5.1. Equations for the formation of ZBUS.  
[11]

| Add p-q                             | Mutual Coupling  | No Mutual Coupling                     |
|-------------------------------------|--|--|
| Branch                              | $Z_{qi} = Z_{pi} + \bar{y}_{pq,rs} (\bar{Z}_{ri} - \bar{Z}_{si})$ $i = 1, 2, \dots, m$ $i \neq q$                                | $Z_{qi} = Z_{pi}$                      |
|                                     | $Z_{qq} = Z_{pq} + \frac{1 + \bar{y}_{pq,rs} (\bar{Z}_{pq} - \bar{Z}_{rs})}{y_{pq,rs}}$  | $Z_{qq} = Z_{pq} + z_{pq,pq}$          |
| Link                                | $Z_{li} = Z_{pi} - Z_{qi} + \frac{\bar{y}_{pq,rs} (\bar{Z}_{ri} - \bar{Z}_{si})}{y_{pq,pq}}$ $i = 1, 2, \dots, m \quad i \neq 1$ | $Z_{li} = Z_{pi} - Z_{qi}$             |
|                                     | $Z_{11} = Z_{p1} - Z_{q1} + \frac{1 + \bar{y}_{pq,rs} (\bar{Z}_{r1} - \bar{Z}_{s1})}{y_{pq,pq}}$                                 | $Z_{11} = Z_{p1} - Z_{q1} + z_{pq,pq}$ |
| Elimination of 1 <sup>th</sup> Node |  |  |
|                                     | $Z_{ij}(\text{modified}) = Z_{ij}(\text{before elimination}) - \frac{Z_{i1} Z_{1j}}{Z_{11}}$                                     |  |
|                                     | $i, j = 1, 2, 3, \dots, m$   |  |

For example, a primitive impedance matrix looks like this for five elements:

$$z^0 = \begin{matrix} & \begin{matrix} 1(1-2) & 2(2-3) & 3(3-4) & 4(1-4) & 5(2-4) \end{matrix} \\ \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{matrix} & \begin{bmatrix} .1+j.5 & j5 & & & \\ j5 & .1+j.5 & & & \\ & & .1+j.5 & j10 & j4 \\ & & j10 & .1+j.5 & j8 \\ & & j4 & j8 & .1+j.5 \end{bmatrix} \end{matrix} \quad y^0 = [z^0]^{-1}$$

where the off diagonal values represent mutual coupling between elements. Using this primitive matrix and the equations in Table 5.1 yields Zbus.

ZBUS.F4 is one of the longest programs in the series. The program asks for the zero-sequence impedance for all loads in the system and the mutual-coupling impedances. If the zero-sequence impedance of a load is not known, the program assigns it the same value as the positive sequence impedance.

All loads that are added are links, and only loads that are added are those of synchronous motors. The subtransient reactance is used instead of its actual impedance since the Z-bus is going to be used for fault calculations. Any link from a bus to the reference bus will cause a fault current. Prefault voltages and currents will be ignored as will all contributions from loads other than synchronous motors. A flow chart follows (Figure 5.2) and a complete program listing in Appendix B.

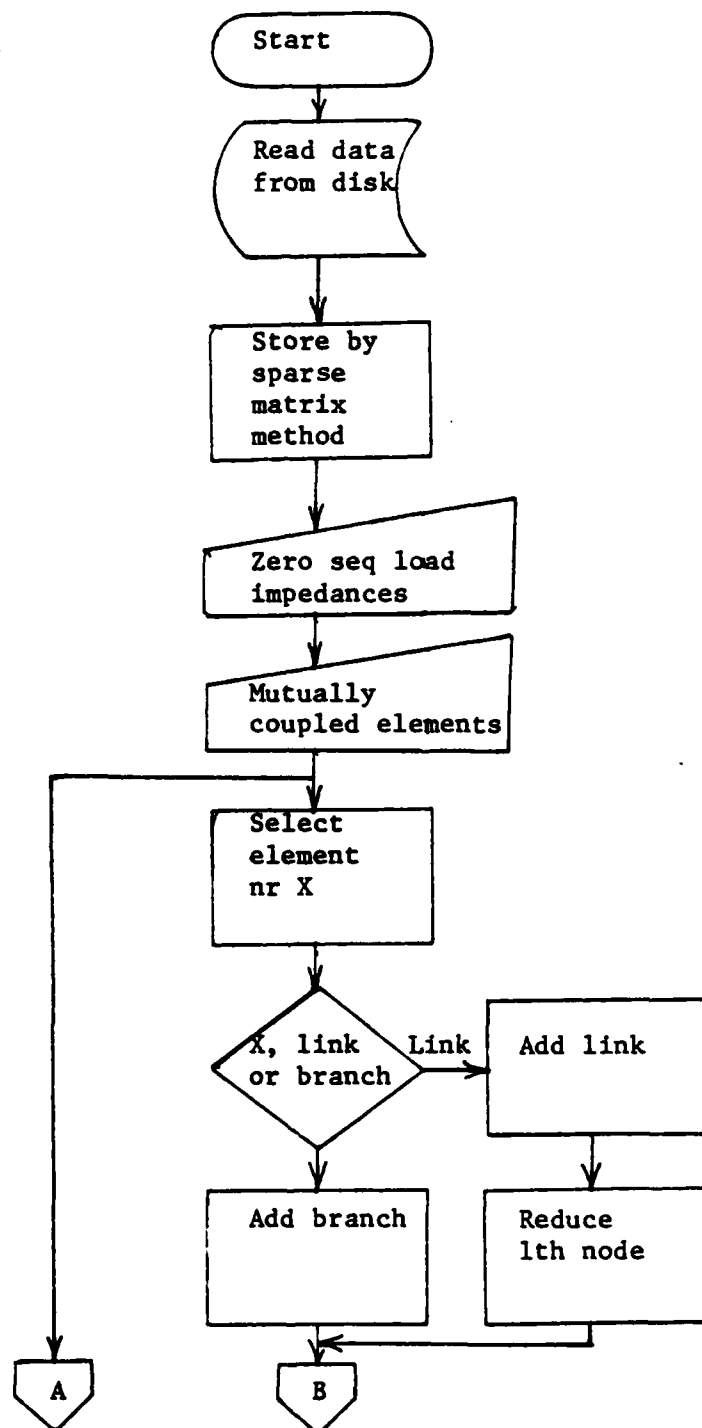


Figure 5.2. Zbus<sup>012</sup> formation flow chart.

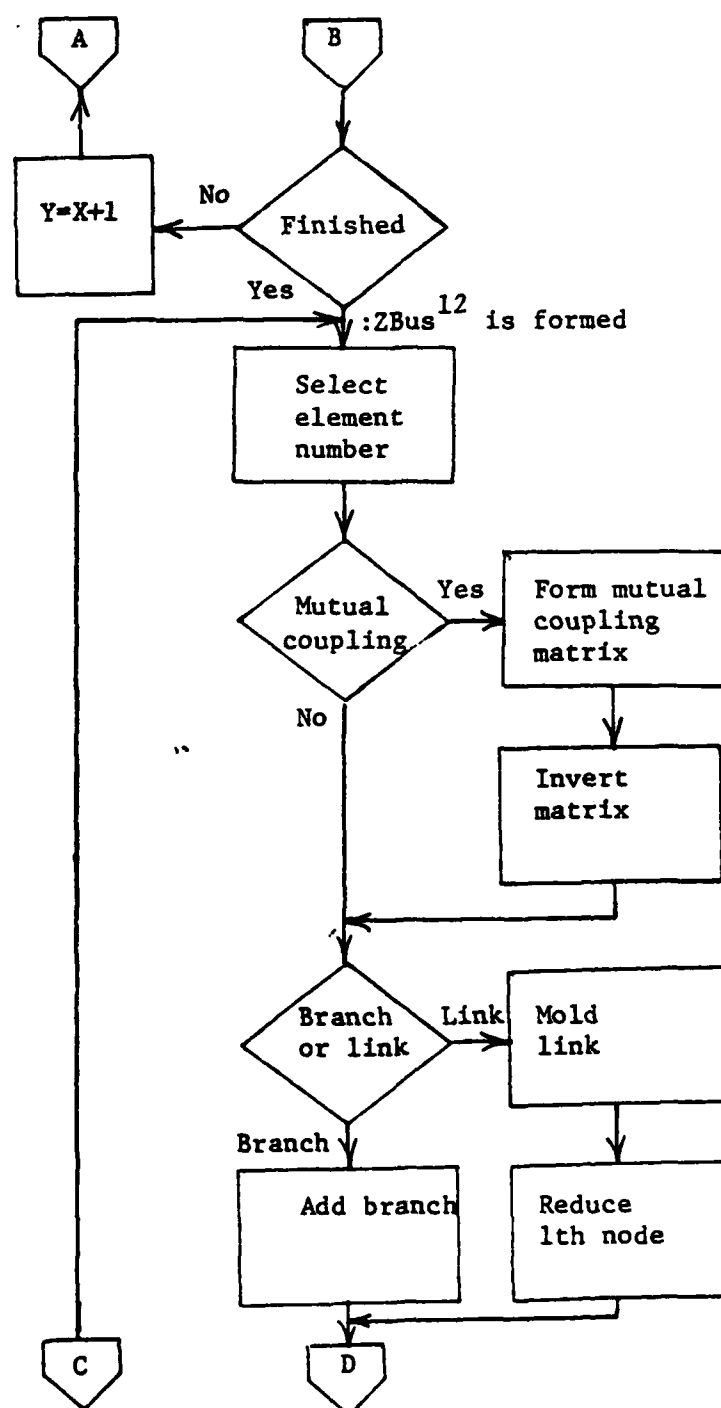


Figure 5.2. Continued.

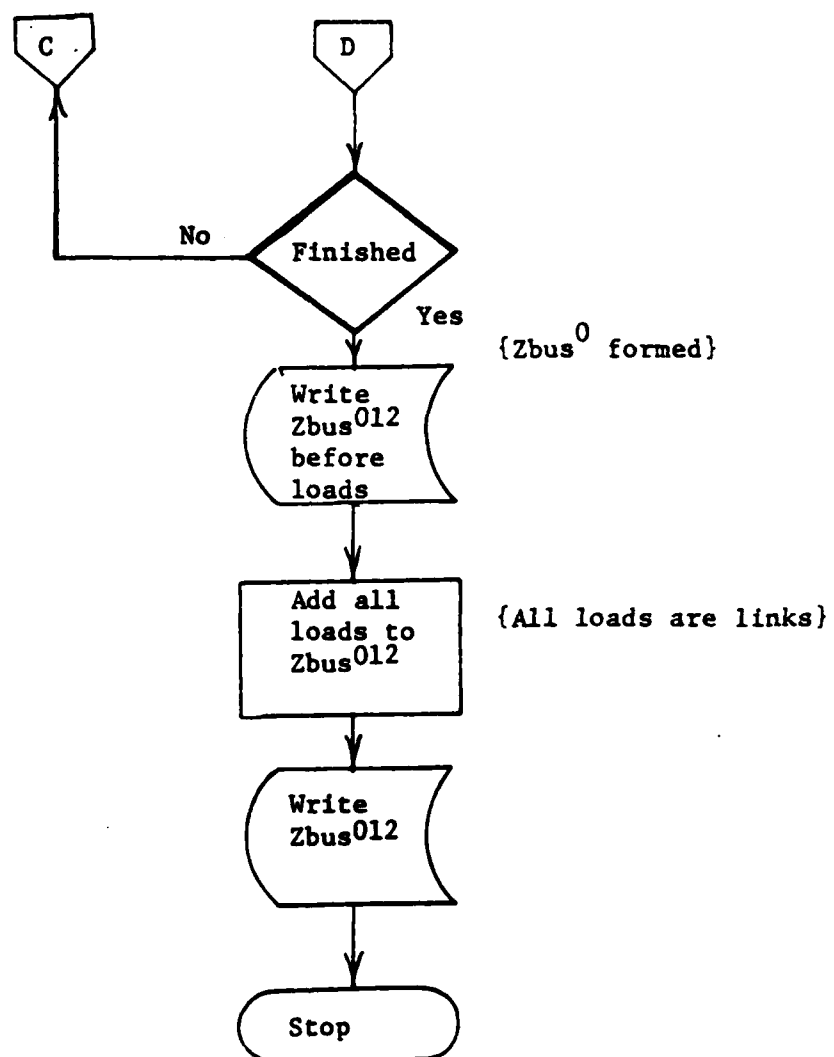


Figure 5.2. Continued.

Summary

$Z_{bus}^{012}$  is formed by algorithm allowing for mutual coupling between elements. The next step in the coordination procedure is to solve for fault currents. This procedure follows in the next chapter.



## 6. FAULT CALCULATIONS

### General

The final program required before executing the coordination program is FALT.F4. This program computes all the possible line-to-ground and three-phase-fault currents and prepares all other load data for entry into the coordination program. The procedure to accomplish this will be discussed in this chapter.

Fault Currents. The equations describing the fault currents need to be derived [12].

Three-Phase Fault. For a fault at bus P:

$$I_{P(F)}^{012} = Y_F^{012} (U + Z_{pp}^{012} Y_F^{012})^{-1} E_{P(0)}^{012} \quad (6.1)$$

where U is unity matrix,  $E_p(0)$  is prefault voltage, and  $Y_F$  is the fault admittance matrix for a three-phase fault.

$$Y_F^{012} = y_F \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad (6.2)$$

Substituting (6.2) into (6.1)

$$\begin{aligned}
 I_{P(F)}^{012} &= y_F \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1+Z_{pp}^0 & & \\ & 1+Z_{pp}^1 y_f & \\ & & 1+Z_{pp}^2 y_{pf} \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ \sqrt{3} \\ 0 \end{bmatrix} \\
 I_{P(F)}^{012} &= y_F \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \frac{1}{1+Z_{pp}^0} & & \\ & \frac{1}{1+Z_{pp}^1 y_F} & \\ & & \frac{1}{1+Z_{pp}^2 y_F} \end{bmatrix} \begin{bmatrix} 0 \\ \sqrt{3} \\ 0 \end{bmatrix} \\
 I_{P(F)}^{012} &= y_F \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{1}{1+Z_{pp}^1 y_F} & 0 \\ 0 & 0 & \frac{1}{1+Z_{pp}^2 y_F} \end{bmatrix} \begin{bmatrix} 0 \\ \sqrt{3} \\ 0 \end{bmatrix} \quad (6.3)
 \end{aligned}$$

Since  $Z_{pp}^1 = Z_{pp}^2$  and  $z_f = 1/y_f$

$$I_{P(F)}^1 = \frac{\sqrt{3}}{z_F + Z_{pp}} \quad I_P^0 = 0 \quad I_P^2 = 0 \quad (6.4)$$

Using the same method the following equations are found [12].

$$E_{P(f)}^1 = \frac{\sqrt{3} z_F E_{Po}}{z_F + z_{pp}} \quad (6.5)$$

and

$$E_{i(f)}^1 = \sqrt{3} (E_{i(0)} - \frac{z_{ip}^{(1)} E_p^{(0)}}{z_f + z_{pp}^{(1)}})$$

$$i \neq p \quad E_i^{0,2} = 0 \quad E_{p(f)}^{0,2} = 0 \quad (6.6)$$

These equations are identical to those found for a three-phase grounded fault [12].

The line-to-ground fault admittance matrix is given by  $Y_F^{012}$  below. Substituting  $Y_F^{012}$  into (6.1) the equations below result [12].

$$Y_F^{012} = \frac{y_F}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix}$$

$$I_P^{012} = \frac{\sqrt{3} E_{p(0)}}{z_{pp}^0 + 2z_{pp}^{(1)} + 3z_F} \quad (6.7)$$

$$E_p^{012} = \frac{\sqrt{3} E_p^0}{Z_{pp}^{(0)} + 2Z_{pp}^{(1)} + 3z_F} \begin{bmatrix} -Z_{pp}^{(0)} \\ Z_{pp}^{(0)} + Z_{pp}^{(1)} + 3z_F \\ -Z_{pp}^{(1)} \end{bmatrix} \quad (6.8)$$

$$E_{i(F)}^{012} = E_{i(0)} \begin{bmatrix} 0 \\ \sqrt{3} \\ 0 \end{bmatrix} - \frac{\sqrt{3} E_p^{(0)}}{Z_{pp}^{(0)} + 2Z_{pp}^{(1)} + 3z_F} \begin{bmatrix} Z_{ip}^{(0)} \\ Z_{ip}^{(1)} \\ Z_{ip}^{(1)} \end{bmatrix} \quad (6.9)$$

$i \neq p$

The value of  $z_F$  is entered from the keyboard when asked by the program. All of the equations are available now to solve for all fault currents. All post-fault bus voltages are solved. Using these bus voltages each element fault current is determined. These currents are stored onto disk so that they may be used in both the coordination and graphing programs.

### Summary

The programs thus far have solved for all load and fault currents but no coordination has been discussed. Now the coordination problem is ready to be addressed. In the chapter that follows, the protective devices for the distribution system will be coordinated.

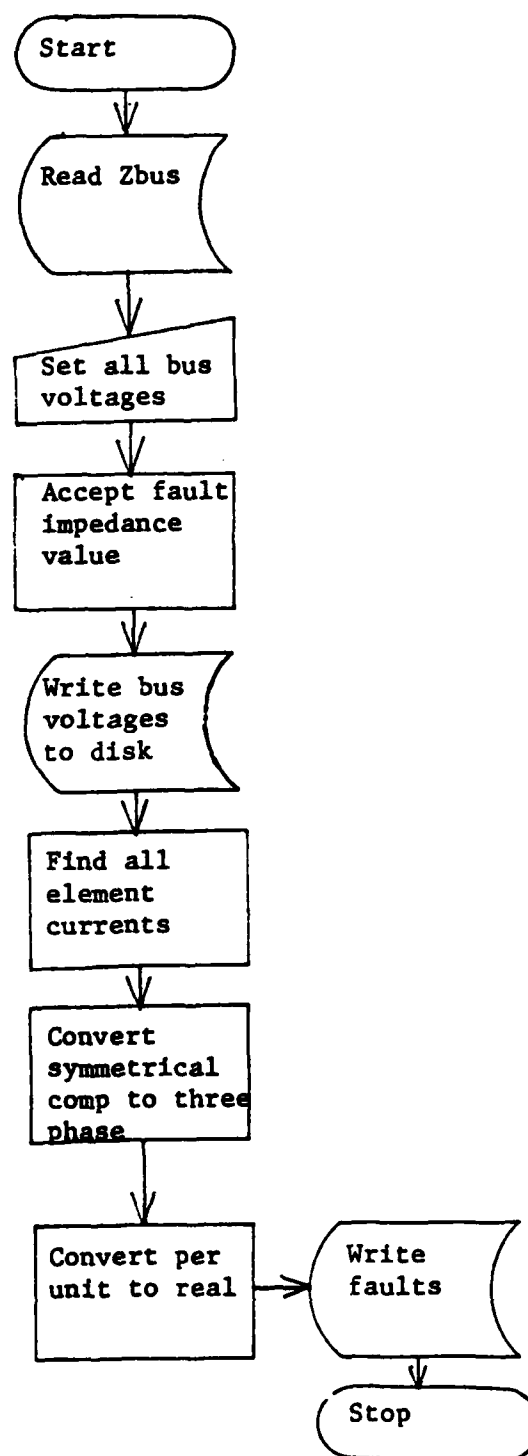


Figure 6.1. Flow chart for FALT.F4.

## 7. PROTECTIVE-DEVICE COORDINATION

### General

In this chapter, the protective-device-coordination problem will be discussed. A computational method is put forward that allows a digital computer to solve the problem.

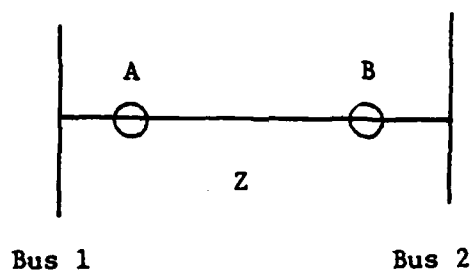
### Device Coordination

One of the best methods to approach coordination is a step by step device selection and setting working from the load toward the source. A load is the best place to start because there is not much flexibility for device setting at a load. The load flow analysis of Chapter 4 provides the overload values for the various loads. This enables a definite overload setting for each device protecting a load. Since overload currents are a primary concern at these buses, all fault settings can be placed at six times the full load currents. This should allow for normal starting currents. Care must be taken so that an instantaneous tripping element will not open under normal starting conditions. From the loads it is a straightforward process to place a line side device curve next to its load side curve to insure that proper coordination is achieved. By taking this approach, each device depends only on one other device.

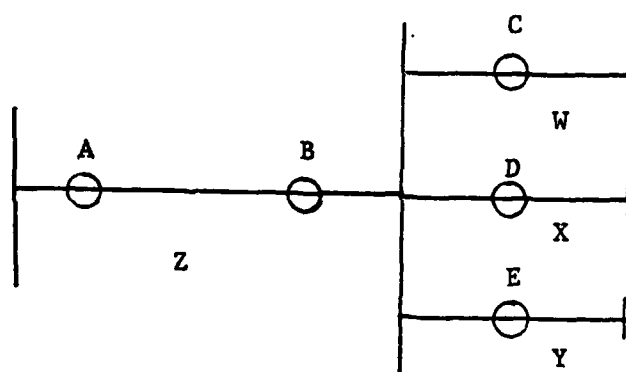
This program is written with the option of entering two devices in each element--one located at each bus. From this approach, obviously two possibilities can occur. Either the device is on the line side of the element or on the load side of the element (Figure 7.1). If it is the line-side device, its setting depends only on the one load-side device. It must be coordinated for the fault current at the load bus and not the line bus [1]. Devices must be coordinated for a minimum possible fault current which will be discussed later.

If the device is on the load side and it does not protect a load, then it must protect a following bus. This device must then be coordinated with all line-side devices connected to the bus it protects. This load-side device must be coordinated for fault currents at the protected bus.

Devices should be set to (1) open under overload conditions, (2) open under minimum fault conditions with proper coordination, and (3) open under maximum fault conditions with proper coordination. Often, however, all three conditions cannot be met simultaneously unless the proper devices are chosen. Criterion (1) is not as important as Criterion (2) or (3) when in the distribution system not at a load bus since an overload condition below fault conditions should not do damage to the wiring. For this reason wire sizes must be checked to insure that upon final coordination they can withstand the overload and fault conditions that can occur [5,13]. At this point it may be necessary to begin the entire coordination procedure again if an element cannot withstand the short-circuit conditions. Allowable short-circuit currents can be checked by using the final coordination graph and the fault currents obtained in FALT.F4.



(a) Coordinating line side device of an element.



(b) Coordinating load side device of an element feeding a bus with load elements connected W, Z, Y.

**Figure 7.1.** Two possibilities for coordination element Z. In Figure (7.1a) coordination device A according to curve device B up to fault bus 2. In Figure (7.1b) coordination device B depending on load flow current element Z. Coordinated with device curves C, D, E, up to fault at Bus 2.



This coordination routine utilizes fault currents and load currents in achieving protective-device coordination. The load currents determine the overload or pickup setting in each device. The coordination problem is then in two parts.

Devices must be coordinated for overload conditions. This provides the most important coordination step for fuses in that they contain no variable fault-protection settings as do relays or molded-case circuit breakers. Also, another reason is that based upon only fault currents and load-side device settings, it is impossible to satisfactorily achieve coordination.

This inability to achieve coordination enters when setting a device that is to protect a bus with other elements attached to that bus as loads. Just laying a line curve next to a load curve with the highest time value at any current value will provide an erroneous answer. This device must be set by determining its overload current value first since this current is the sum of all currents in the load elements that are attached to that bus. Once this point has been established, each load device curve must be polled in turn to insure that the device setting responds to a fault in a load element slower than the load element line side device. The device needs to be coordinated up to the maximum fault current that the device will see. It is possible for this device to see a smaller fault current than that in a load element.

Coordinating a device located at a line-side bus is much simpler since the pickup or overload setting is the same as the load-side device. The line-side device must be coordinated up to the maximum

fault current that will occur at the bus where its load-side device is located. A higher fault current will occur the closer one gets to the line-side device; however, this higher current value will only cause the line-side device protecting the element to respond quicker. The method of coordination will be to first find a load point based on a load flow, and second coordinate the device at any current value up to some maximum fault current such that the line-side device has a longer response time than its load-side device.

Since the program coordinates three different types of devices, nine different possibilities can occur. Each device may be coordinated with one of its own type or one of the other two.

The program structure lends itself well to the use of subroutines. Two of these are SELECT and SETDEV. SELECT chooses a device and sets its own load point, and SETDEV coordinates it.

#### Fuse Selection and Coordination

Due to the large number of fuse sizes available, look-up tables are not as efficient as using polynomial functions to select devices. Once a load current is known, this value is substituted into one function providing the proper device number. This device number is next substituted into two other functions providing the OFFSET and OFFSET 1 values referred to in Chapter 2. Since there are two types of fuses in the program, current-limiting and solid-material boric-acid power fuses, there are six functions used in selecting fuses. These all have the following form:

$$Y = \sum_{j=0}^n a_j X^j \quad (7.1)$$

X will be the logarithm of overload current or device number. Table 7.1 lists the various coefficients  $a_j$ .

After the fuse is selected, it must be coordinated. The program uses the values of OFFSET and OFFSET 1 with the applicable fuse curve to solve for a time value for a set-current value. The program searches for the load-side device to find the highest time value to that current value. If the time value is larger for the size, it is properly coordinated. If not, it increases the fuse size by one, solves for OFFSET and OFFSET 1, and tries again continuing until it has found the proper fuse size.

#### Relay Selection and Coordination

Relays provide the most difficult coordination problem. First a turns ratio for the current transformer (CT) must be chosen. The computer selects the proper tap setting to prevent saturation. It does this by always selecting the highest turns possible while selecting the tap setting on the relay as well [12]. The computation uses a 600/5 CT [13] with tap settings and CO relays [14] with tap settings. This combination of tap setting for the CT and the relay combined with the load current establish the pickup point:

$$\text{Pickup} = \text{Log} [(\text{Turns Ratio CT} \times \text{Turns Ratio Relay})] \quad (7.2)$$

Table 7.1. Fuse-selection coefficients.

| Current to Device                |            | Offset     | Offset 1   |
|----------------------------------|------------|------------|------------|
| <u>Current Limiting Fuses</u>    |            |            |            |
| $a_0$                            | - 11.15221 | .9532      | 1.1619     |
| $a_1$                            | 23.865     | - .046433  | - .110148  |
| $a_2$                            | - 16.487   | .117885    | .10626     |
| $a_3$                            | 2.9288     | - .029352  | - .02249   |
| $a_4$                            | 3.19672    | .00337     | .002452    |
| $a_5$                            | - 1.48877  | - .0001847 | - .0001365 |
| $a_6$                            | .1776431   | .0000039   | .00000304  |
| <u>Solid Material Boric Acid</u> |            |            |            |
| $a_0$                            | 88.1643    | 1.34359    | 1.41734    |
| $a_1$                            | -215.2235  | .151393    | .1585889   |
| $a_2$                            | 188.225    | - .0239735 | - .035007  |
| $a_3$                            | - 69.13403 | .00046627  | .007180    |
| $a_4$                            | 7.4695     | .0004321   | .0008126   |
| $a_5$                            | 1.65757    | .0000182   | - .0000377 |
| $a_6$                            | - .347786  | .0000078   | 0          |

Since relay curves are in units of multiples of pickup this pickup value will be used often. Only the relay pickup has been set, its time dial must be coordinated. Table 7.2 lists the relay-curve coefficients.

Due to the inverse time shape of a relay curve, many points on the curve must be checked with its load-side device to insure that proper coordination exists. The manner in which the family of relay curves are represented simplifies the problem somewhat. A relay operating time of 0.4 seconds is assumed throughout. At each current value, the load-side-device operating time is summed with the relay operating time. If this time is greater than the line-device time, the difference is the relay time-delay setting. Thus, when all currents up to the fault currents are checked, all points on the line-device curve are at least 0.4-seconds higher than all points on its load-side device.

#### Molded Case Circuit Breaker

The molded-case circuit breaker (MCCB) with its different characteristics provides a different set of problems. The MCCB curve cannot be represented by one equation. This device has one set of curves for the thermal element plus another for its magnetic element. The MCCB used in the program is a General Electric type, K-1200. Although there is some difference in the curve shape for the current ratings, 300-1200 A, they are similar enough to be represented as one type. Each MCCB has one curve corresponding to minimum total clearing time and a maximum total clearing time.

Table 7.2. Relay-curve coefficients.

| Relay Number | $a_0$      | $a_1$     | $a_2$     | $a_3$      | $a_4$      |
|--------------|------------|-----------|-----------|------------|------------|
| CO-2 1       | - .4401731 | -3.207952 | 3.098054  | -1.132646  | 0.0        |
| CO-5 2       | 1.415901   | -4.556591 | 7.501177  | -6.484299  | 2.233915   |
| CO-6 3       | .83421     | -4.284002 | 7.005048  | -5.298087  | 1.505842   |
| CO-7 4       | 1.0438914  | -4.308733 | 6.998595  | -5.908597  | 1.894855   |
| CO-8 5       | 1.7617574  | -4.526460 | 3.226049  | - .4676728 | - .2548555 |
| CO-9 6       | 1.476228   | -2.512627 | -1.278763 | 3.363051   | -1.356438  |
| CO-11 7      | 2.897519   | -4.885438 | 4.078362  | -2.517864  | .7629706   |

The magnetic portion of the time-current curve cannot be represented adequately by a polynomial function, but is represented by:

If Current  $\geq$  Magnetic Setting

Minimum Time = 0, Maximum Time = .025 seconds.

As will be seen later, .025-seconds response time is quite fast and usually does not present a problem during later coordination.

The thermal elements of molded-case circuit breakers are susceptible to temperature change so the operating temperature must be entered. The temperature merely shifts the curve to the left or right so it does not affect the curve shape. This offset is added or subtracted from the multiple of current rating when using the thermal curve polynomial functions.

The problem of coordinating the thermal elements is the same as that for fuses. The magnetic element coordination is much simpler in that the magnetic element is set separately. Its load-side device operating time is checked at a current value. If the operating time is greater, the magnetic element setting is increased. The end of the curve for the magnetic element is determined by the maximum fault current at the bus. The total decoupling of the overload from the fault device of a MCCB makes coordination much simpler than the fuse or relay. The more or less proportional-time shape of the curve will ensure that it will be properly coordinated once its proper current rating has been

established. Table 7.3 contains the polynomial coefficients used in the program.

A basic flow chart (Figures 7.2 and 7.3) follows with a complete program listing in Appendix B.

### Summary

In this chapter, the coordination problem was solved to allow fuses, molded-case circuit breakers, and relays to function so as to clear a fault in the area of the fault before interrupting the rest of the distribution system. There is enough flexibility in the program to allow device settings to be changed and checked using the program PLOTD.F4. An example problem would be beneficial at this point to show how to run the programs. In the next chapter, a sample distribution system will be coordinated using the coordination programs.



Table 7.3. Molded-case circuit breaker.

$$\log(\text{time}) = \sum_{n=0}^6 a_n [\log(\text{current}) - (\text{offset} + .1122)]^n - 2$$

$$\log(\text{time}) = \sum_{j=0}^6 a_j [\log(\text{current}) - (\text{offset} + .2315)]^j - 2$$

$$\text{offset} = \log(\text{ckt breaker size})$$

Minimum Time:

$$\begin{aligned} a_0 &= 5.76908 \\ a_1 &= -10.88261 \\ a_2 &= 23.65418 \\ a_3 &= -34.7922 \\ a_4 &= 33.7747 \\ a_5 &= -21.14536 \\ a_6 &= 6.431778 \end{aligned}$$

Maximum Time:

$$\begin{aligned} a_0 &= 5.8596721 \\ a_1 &= -4.3943349 \\ a_2 &= -.50690283 \\ a_3 &= -10.402739 \\ a_4 &= -17.0649561 \\ a_5 &= -13.011543 \\ a_6 &= -4.0107239 \end{aligned}$$

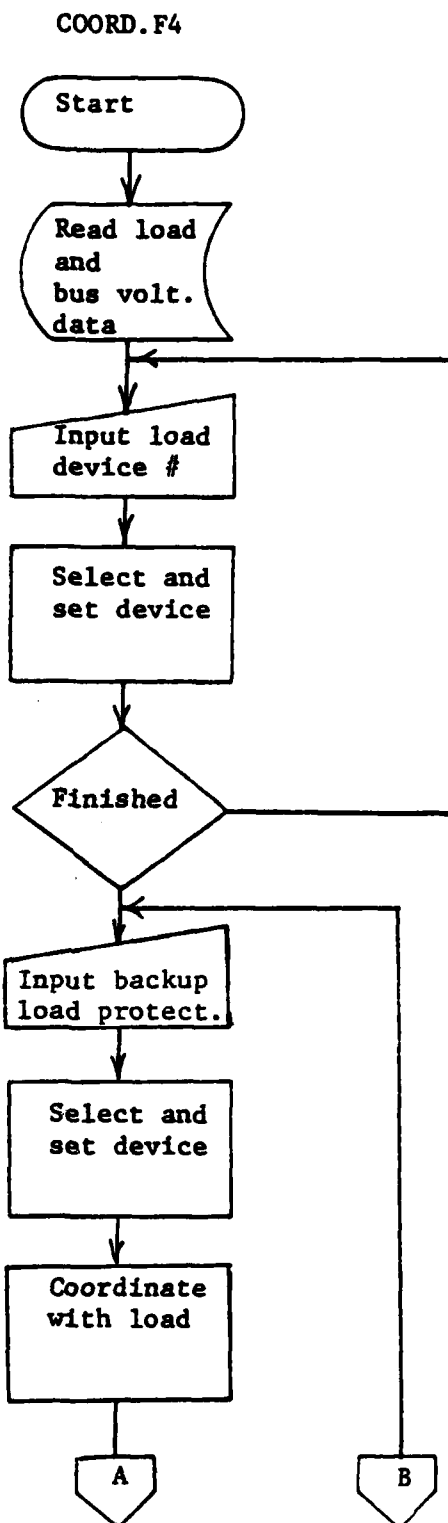


Figure 7.2. Coordination flow chart.

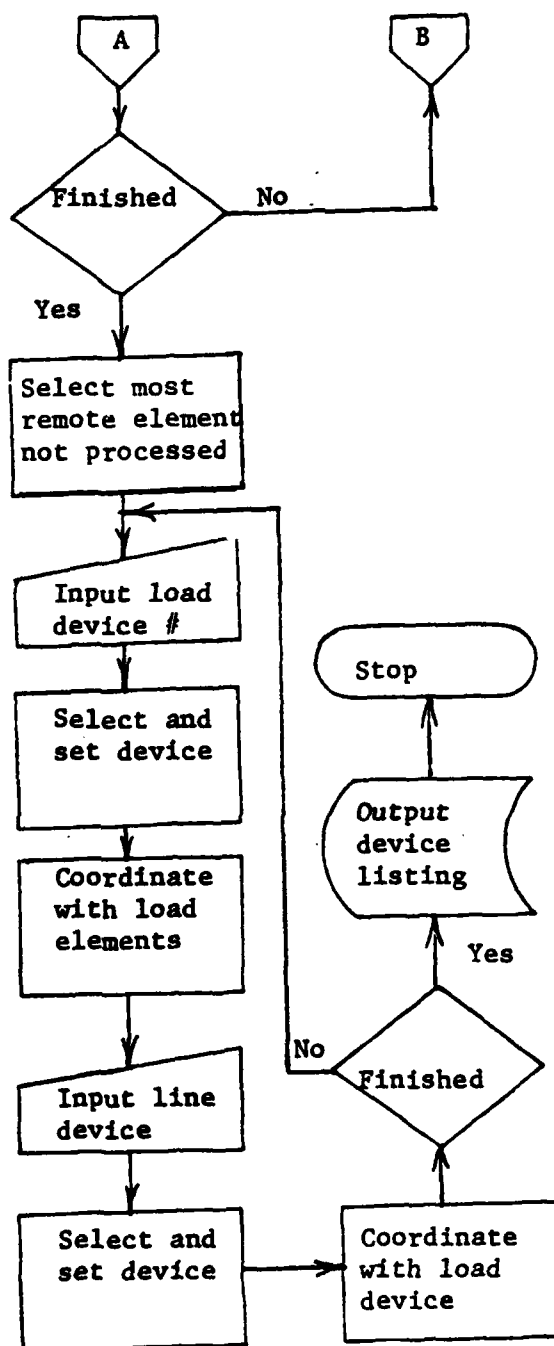


Figure 7.2. Continued.

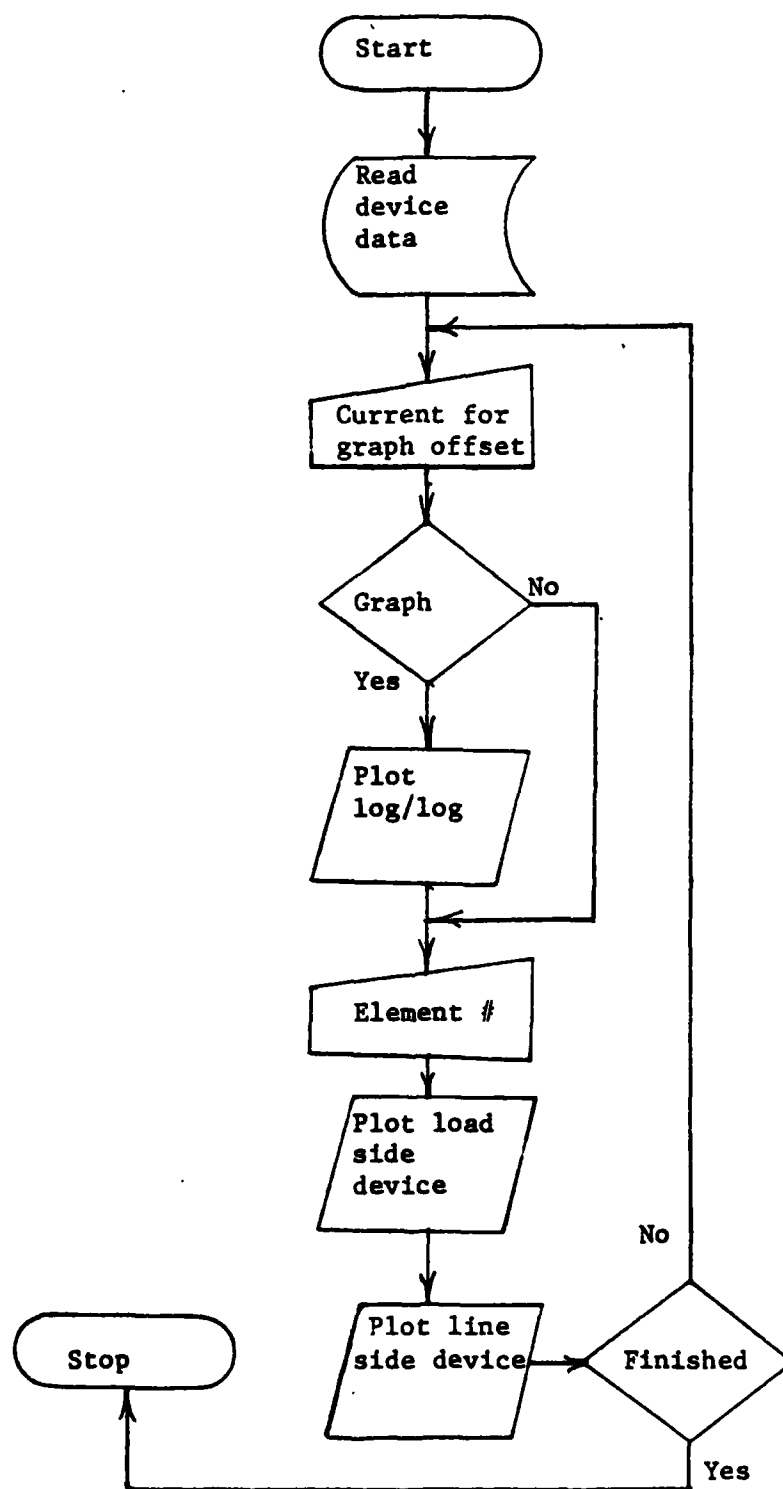


Figure 7.3. Device-graphing flow chart.

## 8. OPERATING THE PROGRAMS

### General

In this chapter the capabilities, limitations, and use of the programs will be described. The example system of Figure 8.1 will be coordinated using these programs.

### One-Line Diagram

INPUT.F4. All data is entered via the keyboard in the format detailed in Chapter 3. Data entry is a straightforward process except when entering transformer data. The program is written for a "Y-Y" configuration. If one or both sides are " $\Delta$ " configured, then a large number must be entered for the transformer neutral impedance "(ZN)" on the bus connected to the  $\Delta$  side. After the program is completed, the zero sequence value for the transformer element containing the transformer may be assigned an arbitrary high value if the transformer wiring is such that there can be no ground current through the element. This is done by changing its value in disk file TEST.DAT (see Appendix C for the file format).

When entering the loads the program asks which type of load to be entered. The various loads are described as:

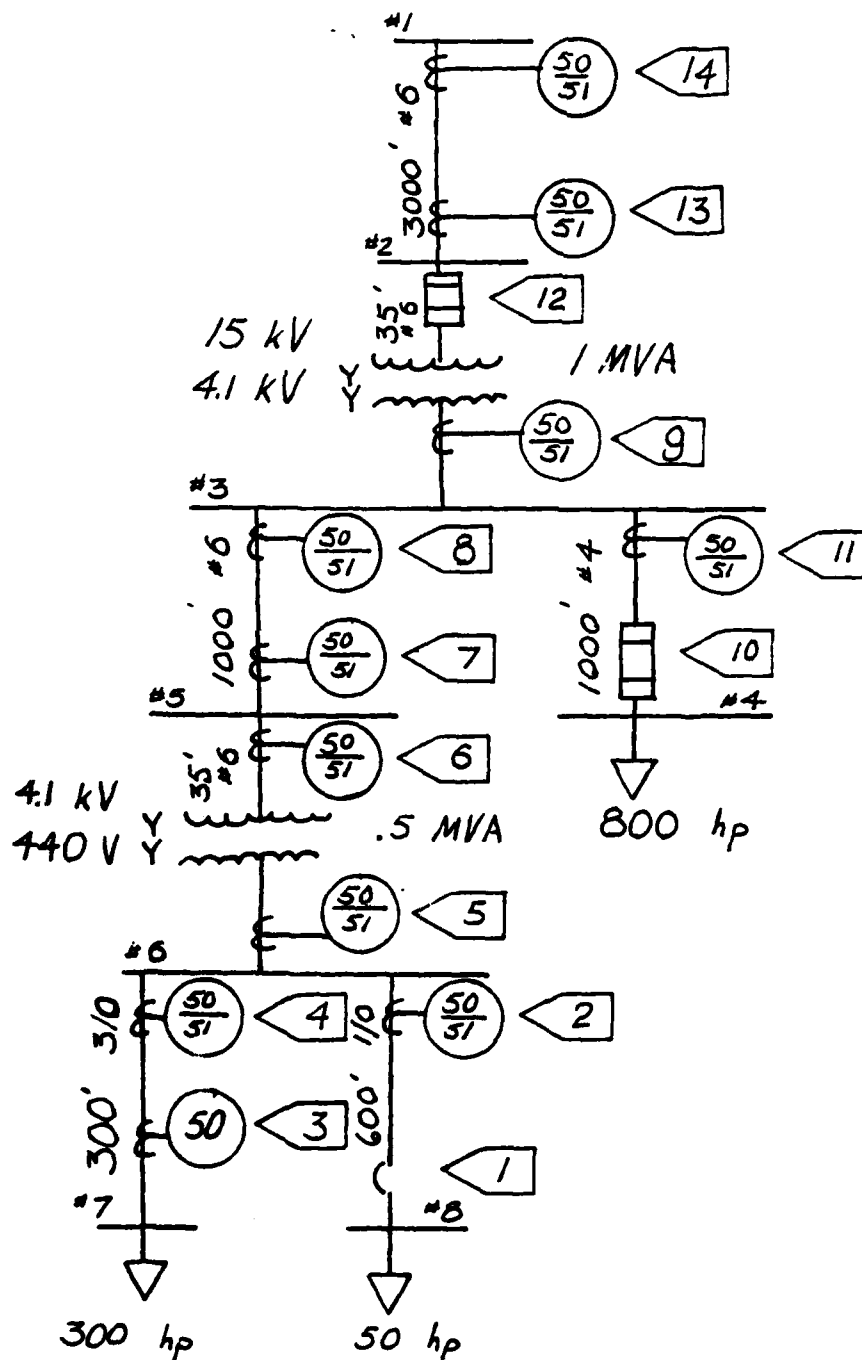


Figure 8.1. One-line diagram of sample system.

HP - Synchronous motor  
HP1 - Assynchronous motor  
VA - In KVA  
CUR - In amperes  
S - No more loads

### Load Flow

INPUT.F4. There are no entries from keyboard for this program. Printing DSK.DAT will provide a load-flow analysis in per-unit values.

### Solution of Fault Currents

ZBUS.F4. In addition to forming  $Z_{bus}^{012}$ , this program allows the input for mutual coupling and for zero-sequence impedance for loads. Mutual coupling tends to increase fault currents in the mutually coupled elements and small neutral-to-ground impedances can create higher line-to-ground fault currents than three-phase faults.

FALT.F4. Besides the solution of fault currents described in Chapter 6, FALT.F4 also allows the input of fault impedances. This can provide an interesting study of the system because the user can go back and place different fault impedances into the fault analysis to see if the protective devices will operate as desired.

### Device Coordination and Plotting

COORD.F4. The program forms a two-dimensional complex matrix called ADEV that contains all the information required to plot all the devices in the system plus all actual settings that are to be made on the devices. An example row 3 in the matrix is 3,(3,4), (-4,2), (1.26,203), (1.03,1.26), (3,667,0), (.67,0), (20,0) in which:

1. For 3, 3 is the row location of the matrix and corresponds to the element number.
2. For (3,4), it is the first column location and is the bus numbers of the element.
3. For (4,2), -4 is a relay type #4; 2 is a current limiting fuse type #2.
4. For (1.26,203), 1.26 is the logarithm of the pickup point; 203 contains the tap information. Two is the tap of the CT, and 03 is the tap of the relay.
5. For (1.03,1.26), 1.03 is the logarithm of the current for the minimum fuse open; 1.26 is the typical fuse open point.
6. For (3.667,0), 3.667 is the magnetic setting of the relay; 0 since the fuse had no magnetic setting.
7. For (.67,0), .67 is the time-dial setting for the relay. The actual time dial setting must be read from the manufacturer's family of relay curves using the formula below at the maximum fault current.



time-dial-setting found = (found-time curve) -

(time-dial 1/2 setting)

8. For (20,0), 20 is the turns ratio of the current transformer.

Device numbers the programs asks for correspond to the devices below:

- 1 - Current limiting fuse
- 2 - Boric fuse high voltage only
- 3 - Molded-case circuit breaker
- 4 - Overcurrent relay

In device 4 the program will ask later what particular type of relay to use from Table 8.1.

Upon completion of coordination, a device listing is typed on the keyboard, and a printout of the same is available by typing: PRINT\*.LPT.

When performing the plot, having a device listing as well as a fault current listing is helpful.

PLOTD.F4. This program plots the devices that were coordinated above. By using a graph, it is possible to visually check coordination. The program arrangement allows the user to change any device setting or size in ADEV.DAT to tailor the coordination to his particular requirements (see Appendix C for the file format). The program uses the lowest

Table 8.1. Overcurrent-relay types.

| Program Type # | Relay Type |
|----------------|------------|
| 1              | CO-2       |
| 2              | CO-3       |
| 3              | CO-4       |
| 4              | CO-5       |
| 5              | CO-6       |
| 6              | CO-7       |
| 7              | CO-11      |

Relay type numbers are listed as negative numbers by the program.

voltage in the system as a base for plotting currents. The user can select any plot offset. This has the effect of plotting only the area of concern. In this way a very detailed graph can be obtained.

Tables 8.1-8.4 provide a listing of program device type numbers to the actual device type and size.

Table 8.5 details what is contained in the various disk locations created by the programs.

To coordinate the devices in Figure 8.1, the procedure begins by entering element data using INPUT.F4. The program asks if data is to be read from disk or from the keyboard. The first element must be entered using the keyboard.

The proper procedure is to group the elements to be entered by wire or cable type as the program only handles one type of wire or cable at a time. When completed with one type, answer zero for all other questions and the computer writes the element data that it has computed on disk in the file RELA.DAT and stops. The new wire type polynomial coefficients are copied into RES.DAT and the program is ready to be run for the new wire type.

The cable coefficients used in the test problem are for mine power cable [5]. The coefficients are listed in Table 8.6.

After selecting keyboard, the base power and volts are entered. The computer then informs the user to begin element data entry. The data format (Chapter 3) is listed to aid the user. For example, the element from bus one to two of Figure 8.1 is entered as follows: 1/2/3000/6. For the element containing the 1 MVA transformer the following is input: 2/3/35/6/.001.005/1/15/4.1. The bus base voltages are

Table 8.2. Current-limiting fuses.

| Program Type # | Limiting Fuses |
|----------------|----------------|
| 1              | 5E             |
| 2              | 7E             |
| 3              | 10E            |
| 4              | 15E            |
| 5              | 20E            |
| 6              | 25E            |
| 7              | 30E            |
| 8              | 40E            |
| 9              | 50E            |
| 10             | 65E            |
| 11             | 80E            |
| 12             | 100E           |
| 13             | 125E           |
| 14             | 150E           |
| 15             | 200E           |

Table 8.3. Boric fuses.

| Program Type # | Size   |
|----------------|--------|
| 16             | 15E    |
| 17             | 20E    |
| 18             | 25E    |
| 19             | 30E    |
| 20             | 40E    |
| 21             | 50E    |
| 22             | 65E    |
| 23             | 80E    |
| 24             | 100E   |
| 25             | 125E   |
| 26             | 150E   |
| 27             | 175E   |
| 28             | 200E   |
| 29             | 250E   |
| 30             | 300E   |
| 31             | 400E   |
| 32             | 2-250E |
| 33             | 2-300E |
| 34             | 2-400E |

Table 8.4. Molded-case circuit breakers.

| Program # | Size      |
|-----------|-----------|
| 34        | 300 amps  |
| 35        | 350 amps  |
| 36        | 400 amps  |
| 37        | 450 amps  |
| 38        | 500 amps  |
| 39        | 600 amps  |
| 40        | 700 amps  |
| 41        | 800 amps  |
| 42        | 1000 amps |
| 43        | 1200 amps |

Table 8.5. Disc files.

---

|            |   |
|------------|---|
| DIGIT.F4:  | Curve-smoothing program                             |
| DEV.F4:    | Numonics input program                              |
| INPUT.F4   | Element data-input program                          |
| LD Flo.F4: | Load-flow program                                   |
| ZBUS.F4:   | Formation of ZBUS <sup>012</sup> program            |
| FALT.F4:   | Solution of fault-current program                   |
| COORD.F4:  | Coordinate device program                           |
| PLOT.D.F4: | Plot device curves                                  |
|            |   |
| RES.DAT:   | Contains X/R line coefficients                      |
| TEST.DAT:  | Contains element and load data in per unit          |
| RELA.DAT:  | Contains element and bus voltage data               |
| XFOR.DAT:  | Contains transformer inrush and withstand values    |
| LOCUR.DAT: | Contains load currents                              |
| DEV.DAT:   | Contains relay coefficients                         |
| DSK.XFR:   | Contains load-flow currents in P.U.                 |
| DSK.DAT:   | Contains load-flow analysis data                    |
| ZBUS.DAT:  | Contains ZBUS <sup>012</sup>                        |
| ZBUS.FOR:  | Contains ZBUS <sup>012</sup> before loads are added |
| MUT.CO:    | Contains mutual coupling data                       |
| FALT.DAT:  | Contains per-unit fault currents                    |
| EFLT.DAT:  | Contains per-unit fault voltages                    |
| LCUR.DAT:  | Contains real values of load-flow currents          |
| FCUR.DAT:  | Contains real values of fault currents              |
| ADEV.DAT:  | Contains coordinated-device listing                 |

---

Table 8.6. Mine power cable polynomial coefficients.

|       | R-resistance             | X-reactance             |
|-------|--------------------------|-------------------------|
| $a_0$ | 0.758690526734D+01       | 0.6731452381407621D-01  |
| $a_1$ | -- .1108155100578006D+02 | - .1408237729509665D-01 |
| $a_2$ | 0.6290760668063740D+01   | - .1721580927352306D-02 |
| $a_3$ | - .1627214281565102D+01  | .6845126542245339D-03   |
| $a_4$ | 0.1604746751660286D+00   | 0.0                     |



input next with the voltage in volts. Upon completion of entry of all bus base voltages, the computer types the computed element value in per unit. The load data is entered next. The program types the data entry format for the user. The 50 hp motor is entered as: 8/50/.85. The only other data to be entered are mutual coupling and zero sequence load impedance in ZBUS.F4 and fault impedance in FALT.F4. The sample problem uses no coupling and a fault impedance of zero. COORD.F4 is run next. The device type desired is entered when asked for by the program. A sample data input is given in Appendix D.

The following is a list of load locations and currents.

Bus number    Load current

|   |             |
|---|-------------|
| 4 | 84.0396680  |
| 4 | 84.0396680  |
| 7 | 293.6613400 |
| 8 | 48.9435570  |

The following is the current flow in the system under full load conditions as found from the load flow analysis.

| Bus | P | to | Bus | Q | Current at P | Current at Q |
|-----|---|----|-----|---|--------------|--------------|
| 1   |   |    | 2   |   | 34.2226440   | 34.2226440   |
| 2   |   |    | 3   |   | 34.2226630   | 125.2048700  |
| 3   |   |    | 4   |   | 88.0372570   | 88.0372570   |
| 3   |   |    | 5   |   | 39.1722710   | 39.1722710   |
| 5   |   |    | 6   |   | 39.1721210   | 365.0129500  |
| 6   |   |    | 7   |   | 313.4835700  | 313.4835700  |
| 6   |   |    | 8   |   | 51.6573760   | 51.6573760   |

The following is the computed fault currents for a 3 phase fault and a line to ground fault.

| Flt | Bs | P | Element | 3 Phase      | Ln to Gnd    |
|-----|----|---|---------|--------------|--------------|
| 2   |    |   | 1       | 9380.7892000 | 7053.9298000 |
| 2   |    |   | 2       | 261.6855700  | 183.7685400  |
| 2   |    |   | 3       | 677.8190200  | 595.4521200  |
| 2   |    |   | 4       | 280.0413400  | 187.2686100  |
| 2   |    |   | 5       | 280.3767000  | 136.2585700  |
| 2   |    |   | 6       | 2226.3547000 | 1496.4606000 |
| 2   |    |   | 7       | 383.7966800  | 270.9381000  |
| 3   |    |   | 1       | 1247.2941000 | 833.3620700  |
| 3   |    |   | 2       | 1247.2997000 | 826.2558200  |
| 3   |    |   | 3       | 846.6528100  | 699.4013200  |

| Flt | Bs | P | Element | 3 Phase       | Ln to Gnd    |
|-----|----|---|---------|---------------|--------------|
| 3   |    |   | 4       | 349.8265300   | 206.0435600  |
| 3   |    |   | 5       | 349.7991000   | 204.2971400  |
| 3   |    |   | 6       | 2780.8159000  | 1648.7648000 |
| 3   |    |   | 7       | 479.3659400   | 302.5682200  |
| 4   |    |   | 1       | 1017.3596000  | 469.6438400  |
| 4   |    |   | 2       | 1017.3546000  | 466.3491300  |
| 4   |    |   | 3       | 4003.0938000  | 2210.2807000 |
| 4   |    |   | 4       | 285.3238300   | 121.9024600  |
| 4   |    |   | 5       | 285.3332800   | 121.3072000  |
| 4   |    |   | 6       | 2268.1567000  | 972.7699300  |
| 4   |    |   | 7       | 391.0159800   | 174.0103800  |
| 5   |    |   | 1       | 881.8973500   | 308.3295700  |
| 5   |    |   | 2       | 881.8899900   | 307.2671700  |
| 5   |    |   | 3       | 598.6094700   | 260.1660700  |
| 5   |    |   | 4       | 3803.2506000  | 1384.1725000 |
| 5   |    |   | 5       | 353.1902700   | 108.5970700  |
| 5   |    |   | 6       | 2807.5742000  | 901.2339600  |
| 5   |    |   | 7       | 483.9912400   | 183.8482000  |
| 6   |    |   | 1       | 791.2624200   | 148.9287400  |
| 6   |    |   | 2       | 791.2645000   | 148.4773900  |
| 6   |    |   | 3       | 537.0808000   | 125.4932500  |
| 6   |    |   | 4       | 3416.9009000  | 668.5896000  |
| 6   |    |   | 5       | 3416.8793000  | 569.4760500  |
| 6   |    |   | 6       | 2839.6040000  | 517.3090900  |
| 6   |    |   | 7       | 489.5244300   | 124.5511200  |
| 7   |    |   | 1       | 350.4617800   | 103.1131400  |
| 7   |    |   | 2       | 350.4624900   | 103.1008700  |
| 7   |    |   | 3       | 237.8819000   | 70.4041400   |
| 7   |    |   | 4       | 1513.3939000  | 445.7008900  |
| 7   |    |   | 5       | 1513.3895000  | 443.9770900  |
| 7   |    |   | 6       | 14273.8630000 | 4235.3970000 |
| 7   |    |   | 7       | 216.8161500   | 64.2673200   |
| 8   |    |   | 1       | 156.6019600   | 23.5717640   |
| 8   |    |   | 2       | 156.6021300   | 23.5401980   |
| 8   |    |   | 3       | 106.3009100   | 16.4766590   |
| 8   |    |   | 4       | 676.2499600   | 102.2285800  |
| 8   |    |   | 5       | 676.2485300   | 100.1874100  |
| 8   |    |   | 6       | 561.9951900   | 84.0730670   |
| 8   |    |   | 7       | 6769.2755000  | 1059.3405000 |

Using the device listing of ADEV.DAT and the plotted curves, it is possible to obtain all device settings.

Device number one is a molded-case circuit breaker. Its size is 300 A and its magnetic trip is on minimum setting.

Device number 10 is a current-limiting fuse number 10.

Device number 12 is a solid-material high-voltage boric fuse number 24.

The relay data follows:

| <u>Device<br/>Number</u> | <u>Type<br/>Number</u> | <u>Ct</u> | <u>Tap</u> | <u>Time<br/>Dial</u> | <u>Magnetic</u> |
|--------------------------|------------------------|-----------|------------|----------------------|-----------------|
| 3                        | 1                      | 3 (120)   | 7          | 1/2                  | ---             |
| 4                        | 1                      | 3         | 8          | 8                    | 6               |
| 5                        | 3                      | 3         | 14         | 5                    | 6               |
| 6                        | 4                      | 3         | 3          | 4                    | 6               |
| 7                        | 5                      | 3         | 4          | 6                    | 6               |
| 8                        | 5                      | 3         | 5          | 6                    | 6               |
| 9                        | 6                      | 3         | 6          | 10                   | 5.2             |
| 2                        | 1                      | 3         | 13         | 5                    | 5.64            |
| 11                       | 1                      | 3         | 4          | 10                   | 6               |
| 13                       | 7                      | 3         | 7          | 2                    | 6               |
| 14                       | 2                      | 3         | 8          | 1/2                  | 6               |

The magnetic trip of device number 9 had to be reduced after coordination to allow the device 12 to set properly to provide protection for the 1 MVA transformer. The graphs that follow show the devices plotted to the lowest voltage in the system, 440 V. All the graphs were computer generated. The first graph shows how a one-line computer diagram would be placed to aid in understanding the graphs.

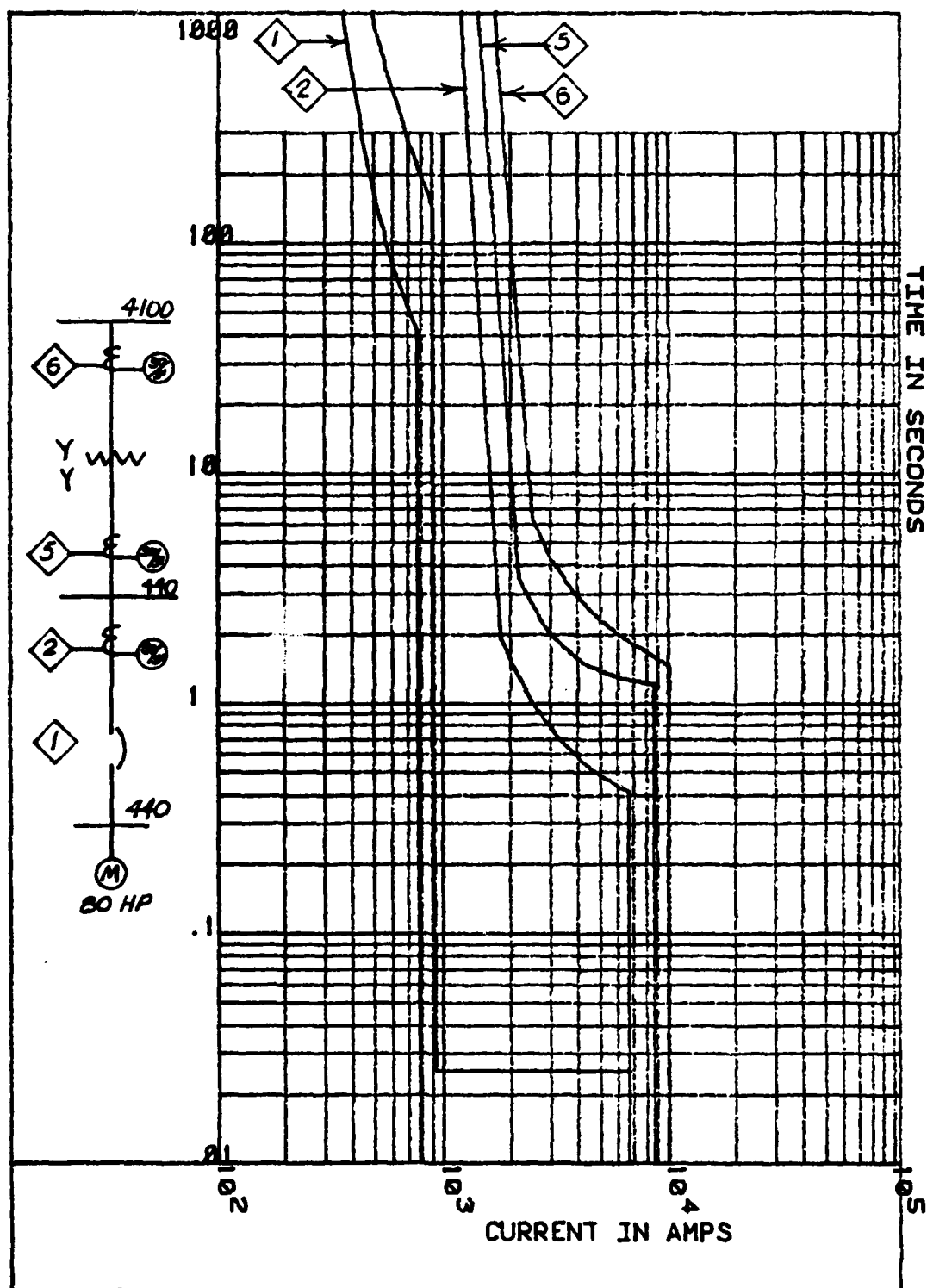


Figure 8.2. Example coordination plot.

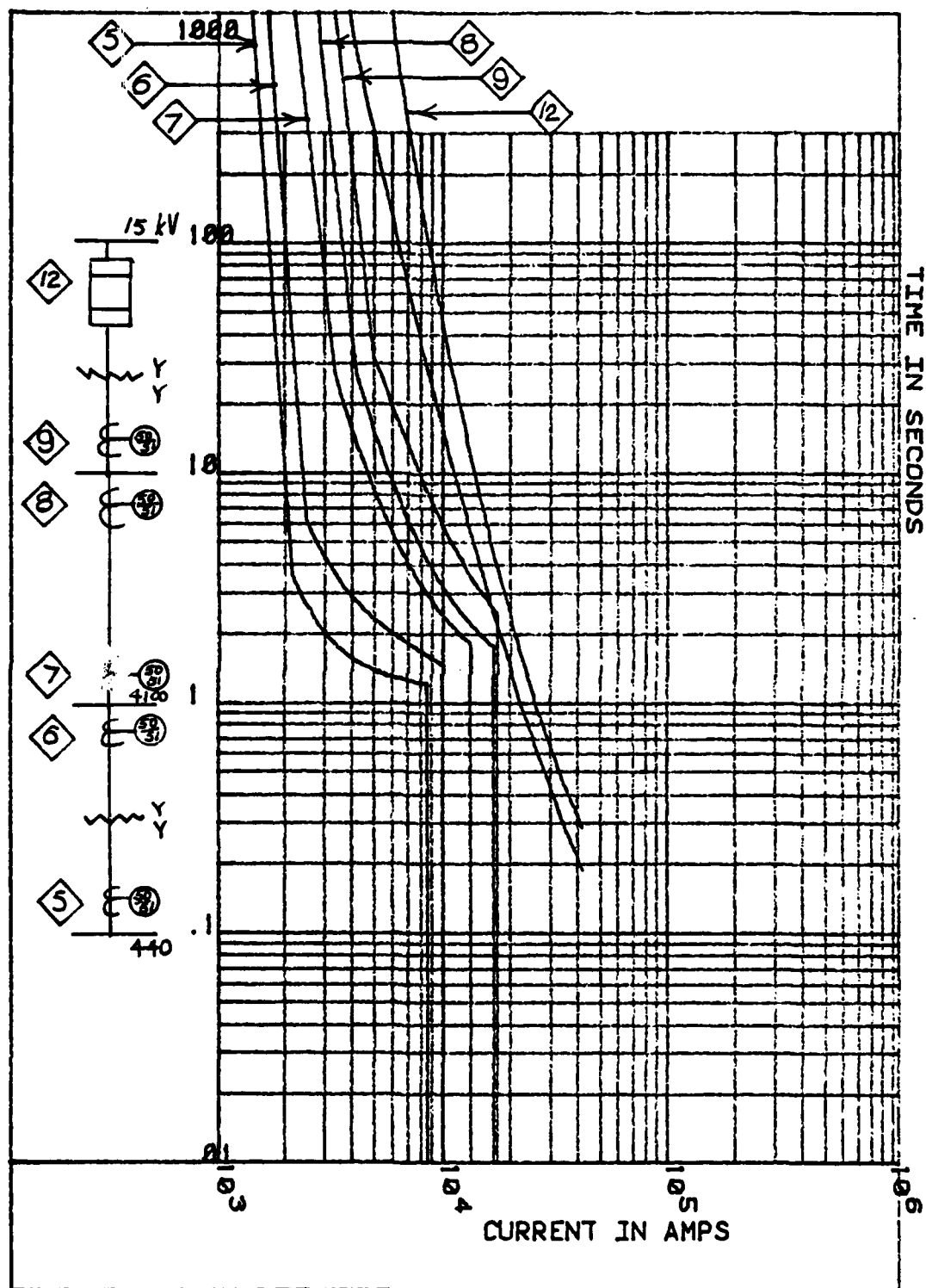


Figure 8.2. Continued.

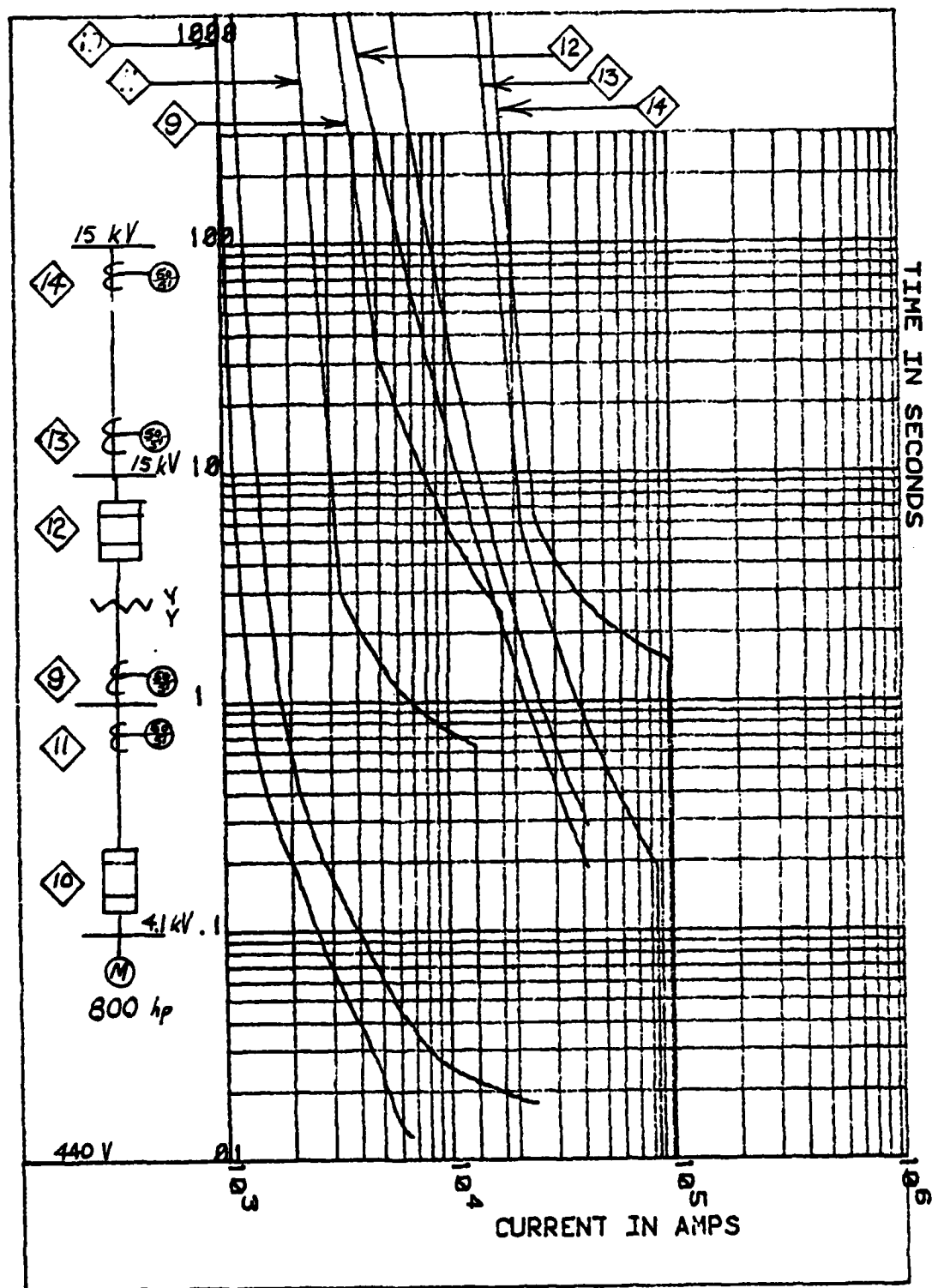


Figure 8.2. Continued.

### Summary

The sample distribution system of Figure 8.1 was coordinated using the coordination programs. Using the device-plotting program PLOTD.F4 this coordination was checked to see if the computer generated coordination was satisfactory to the user.

During the research for this thesis, many observations were made and many features could be added to these programs in the future. This will be discussed in the chapter that follows.



## 9. CONCLUSIONS

In this thesis the author set out to represent a one-line distribution system in a per-unit system and to solve for three-phase and line-to-ground faults and to perform a load-flow analysis. The various protective devices-response curves needed to be represented by polynomial functions. These requirements were fulfilled using the methods detailed in Chapters 2-7.

The last task was to develop a computer procedure to coordinate a distribution system's protective devices. Fuses, molded-case circuit breakers, and relays were coordinated and their coordination graphs were plotted. There are many extensions for further work that could be done. These extensions will be discussed later.

While working with the various programs, several observations have proved useful when performing coordination. Coordination should not be an afterthought in designing a distribution system. It is easy to design a system that is impossible to coordinate correctly. A radial system is easier to coordinate. Moving from a load toward the source, the time-current curves shift to higher current-time responses so that when finally arriving at a transformer, providing proper transformer protection and coordination simultaneously may be impossible.

Coordination of the thermal-tripping elements of molded case circuit breakers is very difficult due to the difference between the minimum and maximum tripping time curves. Coordination of these

devices is best done manually with some overlap of the thermal time curves. The magnetic elements could then be adjusted to provide proper fault coordination. Those manually adjusted devices can be added to ADEV.DAT and be checked using PLOT.F4.

In systems with different voltages, the transformers should be of different sizes so that the smaller sizes are on the load side. This will allow proper coordination and protection. Relays are preferable to other types of protection on the high-voltage parts of the system in that their response can be controlled.

#### Recommendations for Further Work

1. Using an analog computer and the programs presented here, an entire distribution and generation system could be looked at in detail. A transient-stability study would show the effect of various device settings.
2. The INPUT.F4 program could be enlarged to automatically account for different transformer configurations.
3. Additional devices could be added easily to the program. The program allows up to twenty different relay types. The additional coefficient data is merely entered in disk DEV.DAT. Additional molded-case circuit breakers would be slightly more difficult in that it would require some program modification.

4. The plotting program could be enlarged to include drawing a one-line diagram in the space provided and adding other data directly on the graph.
5. The program could be expanded for the case of having one device in an element.

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## APPENDIX A

### CURVE-SMOOTHING PROGRAMS

```

C      TITLE:DIGIT.F4;CREATES FILES FROM DATA
      USING NUMONICS ARM
*****
1      TYPE 5
5      FORMAT(' INPUT DEVICE NR..')
      ACCEPT 8,IDEV
8      FORMAT(I)
      OPEN(UNIT=IDEV)
      TYPE 10
10     FORMAT(' INPUT X-AXIS DIMENSION,Y-AXIS
      DIMENSION'/'..,')
      ACCEPT 15,XAX,YAX
15     FORMAT(2F)
      TYPE 20
20     FORMAT(' INPUT LENGTH PER LOG10;X,Y..')
30     ACCEPT 35,XL,YL
35     FORMAT(2F)
      XAX=100*XAX/XL
      YAX=100*YAX/YL
      CALL OPEN(30,'DEVICE','NUM','MODE','IMAGE',
1'ACCESS','SEQIN','BUFFERS',4)
      CALL NUMRES(30,4)
      CALL LOCK(1,1)
100    READ(30,END=200) IDATA
      IX=(IDATA/"1000000).AND."37777
      IY=IDATA.AND."37777
      IFLAGS=(IDATA.AND."740000)/"40000
      X=IX/XAX
      Y=IY/YAX
      WRITE(IDEV,150)IFLAGS,X,Y
150    FORMAT(I,2F)
      GO TO 100
200    CALL NUMCLO
      CALL UNLOCK(1,1)
      CLOSE(UNIT=IDEV)
      TYPE 210
210    FORMAT(' CONTINUE?..,')
      ACCEPT 220,IC
220    FORMAT(I)
      IF(IC.EQ.0)GO TO 1
      STOP
      END

```

```

*****
C      CURVE FITTING PROGRAM:DEV.F4
*****
      INTEGER L(7),MM(7)
      REAL X(100),YS(100)
      REAL*8 YM(100),G(7,7),U(7),A(0/6),GG(7,7),ERROR(100)
      TYPE 100
100    FORMAT(1X,'CHOOSE DIMENSION OF FIT  '$)
      ACCEPT 110,ND
110    FORMAT(I)
      TYPE 120
120    FORMAT(1X,'CHOOSE NO. OF POINTS  '$)
      ACCEPT 110,M
      TYPE 130
130    FORMAT(/'CHOOSE INPUT FILES'/' ... ,  '$)
      ACCEPT 110,IUNIT1
      DO 140 I=1,M
      READ(IUNIT1,135)J,X(I),YS(I)
135    FORMAT(I,2F)
      YS(I)=ALOG10(YS(I))
140    CONTINUE
      DO 10 K=1,M
      DO 10 I=1,ND
      U(I)=U(I)+YS(K)*X(K)**(I-1)
      DO 10 J=1,ND
      G(I,J)=G(I,J)+X(K)**(I+J-2)
10    CONTINUE
      CALL DMINV(G,7,ND)
      DO 20 I=0,ND-1
      DO 20 J=1,ND
      A(I)=A(I)+G(I+1,J)*U(J)
20    CONTINUE
      DO 30 I=1,M
      DO 30 J=0,ND-1
      YM(I)=YM(I)+A(J)*X(I)**J
30    CONTINUE
      DO 40 I=1,M
      SQUERR=SQUERR+(YS(I)-YM(I))**2
40    TYPE 160,SQUERR
160    FORMAT(' THE INTERGRAL-SQUARED ERROR IS:  ',E)
      OPEN(UNIT=40,FILE='A.DAT')
      WRITE(40,170)A
      CLOSE(UNIT=40)
170    FORMAT(D)
      TYPE 99,IUNIT1
99    FORMAT(' IUNIT=',I)
      DO 50 I=1,M
      ERROR(I)=DABS((YM(I)-YS(I))/YS(I))
      OPEN(UNIT=41,FILE='YINOUT.DAT')
      WRITE(41,180)(X(I),YS(I),YM(I),ERROR(I),I=1,M)
180    FORMAT(2F,2D)

```



```

      CLOSE(UNIT=41)
      STOP
      END
C      TITLE:DMINV;SUBROUTINE TO INVERT A REAL SQUARE
MATRIX DOUBLE
C      PRECISION
      SUBROUTINE DMINV(A,MDIM,N)
      REAL*8 A(MDIM,N)
      INTEGER L(100),M(100)

C
C      CONVERTED FROM SSP ROUTNE MINV
C
      DOUBLE PRECISION BIGA,HOLD
      DO 80 K=1,N
      L(K)=K
      M(K)=K
      BIGA=A(K,K)
      DO 20 J=K,N
      DO 20 I=K,N
10      IF(DABS(BIGA)-DABS(A(I,J))) 15,20,20
15      BIGA=A(I,J)
      L(K)=I
      M(K)=J
20      CONTINUE
      J=L(K)
      IF(J-K) 35,35,25
25      DO 30 I=1,N
      HOLD=-A(K,I)
      A(K,I)=A(J,I)
30      A(J,I)=HOLD
35      I=M(K)
      IF(I-K) 45,45,38
38      DO 40 J=1,N
      HOLD=-A(J,K)
      A(J,K)=A(J,I)
40      A(J,I)=HOLD
45      DO 55 I=1,N
      IF(I-K) 50,55,50
50      A(I,K)=A(I,K)/(-BIGA)
55      CONTINUE
      DO 65 I=1,N
      HOLD=A(I,K)
      DO 65 J=1,N
      IF(I-K) 60,65,60
60      IF(J-K) 62,65,62
62      A(I,J)=HOLD*A(K,J)+A(I,J)
65      CONTINUE
      DO 75 J=1,N
      IF(J-K) 70,75,70
70      A(K,J)=A(K,J)/BIGA
75      CONTINUE

```

```
      A(K,K)=(1.0000000)/BIGA
80      CONTINUE
      K=N
100     K=K-1
      IF(K) 150,150,105
105     I=L(K)
      IF(I-K) 120,120,108
108     DO 110 J=1,N
      HOLD=A(J,K)
      A(J,K)=-A(J,I)
110     A(J,I)=HOLD
120     J=M(K)
      IF(J-K) 100,100,125
125     DO 130 I=1,N
      HOLD=A(K,I)
      A(K,I)=-A(J,I)
130     A(J,I)=HOLD
      GO TO 100
150     RETURN
      END
```

AD-A134 053

A COMPUTATIONAL PROCEDURE FOR THE PROTECTION OF  
INDUSTRIAL POWER SYSTEMS(U) PENNSYLVANIA STATE UNIV  
UNIVERSITY PARK DEPT OF ELECTRICAL ENGINEERING  
C N SALMOND NOV 81

2/2

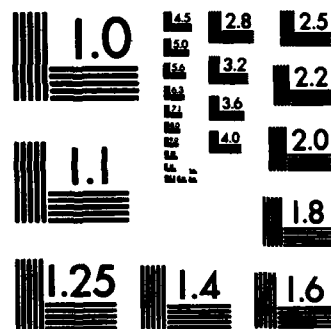
UNCLASSIFIED

F/G 10/2

NL

END

FILED



MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

**APPENDIX B****COORDINATION AND PLOTTING PROGRAMS**

```

*****
C      INPUT.IT INPUTS DATA FROM A TERMINAL, PLACES IN
C      THE PROPER FORMAT FOR OTHER PROGRAMS
*****
C
C
      DIMENSION
L(30,30,2),PU(30,30,1),RES(30,30,2),E(30),XL(30,30,2)
      DIMENSION
S(300),ZER(30,30,2),RC(7),XC(7),ZG(30),XD(30)
      COMPLEX T1,TPU,PU,S,S1,PU1,PZ,CUR,ZER,ZG
      REAL*8 A(7),AA(7)
      REAL L
*****
C      IF THE PROGRAM HAS ALREADY BEEN RUN ONCE ALL DATA
C      NEED NOT BE ENTERED AGAIN
*****
      TYPE 3
3      FORMAT(' DO YOU WANT TO READ DATA FROM A FILE OR
FROM KYBRD?'/
      2' <CR>FOR INPUT FROM TTY,1 FOR READ...')
      ACCEPT 11,I
      IF(I.NE.0)GO TO 400
*****
C      INPUT OF DATA ON LINES
*****
      TYPE 5
5      FORMAT(2X,'ENTER THE PROBLEM BASE IN MVA')
      ACCEPT 10,ZBASE
      TYPE 6
6      FORMAT(2X,'ENTER THE PROBLEM BASE IN KV')
      ACCEPT 10,EBASE
10     FORMAT(F)
11     FORMAT(I)
      GO TO 14
*****
C      PROGRAM RETURNS HERE AFTER READING DATA AT 400
*****
12     TYPE 13
13     FORMAT(' OLD DATA IS ENTERED,READY FOR NEW LINE
DATA...')
      ACCEPT 11,I
14     TYPE 15
15     FORMAT(/,2X,'ENTER ELEMENT DATA AS
FOLLOWS:BUS()TO()(LENGTH)
      1(SP)SIZE',/,2X,'(TRANSFORMER
IMPEDENCE(P.U.))(TRANSFORMER SIZE
      2IN MVA) SP',/, 2X,'(TRANSFORMER HIGH VOLTAGE IN KV)
SP',/,
      3(TRANSFORMER LOW VOLTAGE IN KV]...,'/)
*****

```

C        THESE TWO FILES CONTAIN COEFFICIENT DATA FO 40 BELOW  
 C        THEY ARE CREATED USING THE CURVE FITTING  
 PROGRAM:CURV.F4

\*\*\*\*\*

```

      OPEN(UNIT=40,FILE='RES.DAT')
      OPEN(UNIT=35,FILE='XFOR.DAT')
      READ(40,20)(A(I),I=1,7)
      READ(40,20)(AA(I),I=1,7)
20      FORMAT(D)
      DO 21 I=1,7
      RC(I)=A(I)
      XC(I)=AA(I)
21      CONTINUE
      CLOSE(UNIT=40)
      CLOSE(UNIT=41)
22      ACCEPT 24,I,J,XLL,WIR,11,PS1,TVH,TVL
24      FORMAT(2I,7F)
      IF(I.EQ.0) GO TO 110
      TYPE 26
      JJ=1
26      FORMAT('  PARALLEL LINE    1 TO 3...','$)
      ACCEPT 27,JJ
27      FORMAT(I)
      IF(JJ.EQ.0)JJ=1
      L(I,J,JJ)=XLL
      IF(WIR.EQ.140)GO TO 31
      IF(WIR.EQ.130)GO TO 32
      IF(WIR.EQ.120)GO TO 33
      IF(WIR.EQ.110)GO TO 34
      SA=WIR
      SB=WIR
      IF(SA.LT.37)GO TO 35
      GO TO 40
31      SA=-3
      GO TO 35
32      SA=-2
      GO TO 35
33      SA=-1
      GO TO 35
34      SA=0
      GO TO 35

```

\*\*\*\*\*

C        CONVERSION FROM AWG TO MCM

\*\*\*\*\*

```

35      SC=1.1229**(36-SA)
      SD=.005*SC
      SE=SD**2
      SB=1000*SE

```

\*\*\*\*\*

C        FORMULAE FOR LINE RESISTANCE AND REACTANCE

\*\*\*\*\*

```

40
RES(I,J,JJ)=RC(1)+RC(2)*(ALOG10(SB))+RC(3)*(ALOG10(SB
**2))+
1RC(4)*(ALOG10(SB)**3)+RC(5)*(ALOG10(SB)**4)+RC(6)*(A
LOG10(SB
2**5)+RC(7)*(ALOG10(SB)**6)

XL(I,J,JJ)=XC(1)+XC(2)*(ALOG10(SB))+XC(3)*(ALOG10(SB
**2))+

1XC(4)*(ALOG10(SB)**3)+XC(5)*(ALOG10(SB)**4)+RC(6)*(A
LOG10(SB
2**5)+XC(7)*(ALOG10(SB)**6)
TYPE 50,RES(I,J,JJ),SA,SB,XL(I,J,JJ)
50 FORMAT(2X,'LINE RES. ',3F,/, 'LINE REACT..',F)
IF(CABS(T1).EQ.0)GO TO 85
PU(I,J,JJ)=T1*(ZBASE/TS1)*((TVH/EBASE)**2)
TYPE 55,I,J
55 FORMAT(' INPUT TRANSFORMER ZN IN P.U. REFER TO BUS
SIDE,(BUS
1',I3,')SP(BUS ',I3,')...')
ACCEPT 60,S1,PU1
60 FORMAT(4F)
TV=TVH*1E3
ZG(I)=S1*(ZBASE/TS1)*((EBASE/TVH)**2)
ZG(J)=PU1*(ZBASE/TS1)*((EBASE/TVL)**2)
CURB=TS1*1E6/TV
TINRSH=12*CURB
TWST1=25*CURB
TWST2=14.4*CURB
WRITE(35,70)I,J,TINRSH,TWST1,TWST2,TS1
70 FORMAT(2I,4F)
85 IF(IMAX.GT.I) GO TO 90
IMAX=I
90 IF(JMAX.GT.J) GO TO 100
JMAX=J
100 ZER(I,J,JJ)=CMPLX(0.0,XL(I,J,JJ))
TYPE 102,ZER(I,J,JJ),SS1
102 FORMAT(3F)
GO TO 22
110 OPEN(UNIT=31,FILE='RELA.DAT')
OPEN(UNIT=32,FILE='TEST.DAT')
OPEN(UNIT=33,FILE='LOCUR.DAT')
IF(IMAX.LT.JMAX) GO TO 115
IB=IMAX
GO TO 118
115 IB=JMAX
*****
C BUS VOLTAGES ARE INPUT
*****

```



```

118      DO 120 I=1,IB
        TYPE 119,I
119      FORMAT(' INPUT BUS',I3,'VOLTAGE....',F,$)
        ACCEPT 10,E2
        IF(E2.EQ.0)GO TO 121
        E(I)=E2
120      CONTINUE
121      TYPE 122
122      FORMAT(/,2X,'DATA IS ACCEPTED AND A LIST FOLLOWS')
        TYPE 125,ZBASE
125      FORMAT(2X,'PROBLEM BASE IN MVA... ',F)
        WRITE(31,126)ZBASE,EBASE,IB
126      FORMAT(2F,I)
        E1=E(I)/(EBASE*1E3)
        WRITE(32,128),IB,E1
128      FORMAT(I,2F)
        DO 135 I=1,30
        DO 133 J=1,30
        DO 133 JJ=1,2
        IF(L(I,J,JJ).EQ.0)GO TO 133
        NN=NN+1
        PZ=(CMPLX(RES(I,J,JJ),XL(I,J,JJ)))*(.001*L(I,J,JJ))
        PZZ=(ZBASE*1E6)/(E(I)**2)
        PZ=PZ*PZZ
        T1=PZ+PU(I,J,JJ)
        ZER(I,J,JJ)=ZER(I,J,JJ)*PZZ*(.001*L(I,J,JJ))+T1
        TYPE 130,NN,L(I,J,JJ),T1
130      FORMAT(2X,'ELEMENT ',I3,5X,'LENGTH',F,/,
        11X,'TRANSFORMERPER UNIT IMPEDENCE PLUS LINE
        IMPEDENCE',2F)

        WRITE(31,131)I,J,JJ,L(I,J,JJ),RES(I,J,JJ),PU(I,J,JJ),
        XL(I,J,JJ)
        1,ZG(I),ZG(J)
131      FORMAT(3I,9F)
        WRITE(32,132)NN,I,J,JJ,T1,ZER(I,J,JJ),ZG(I),ZG(J)
132      FORMAT(4I,8F)
133      CONTINUE
135      CONTINUE
        WRITE(31,136)
        WRITE(32,136)
136      FORMAT(' 0 0 0 0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0')
        DO 138 I=1,IB
        WRITE(31,137)I,E(I)
137      FORMAT(I,2F)
138      CONTINUE
        WRITE(31,139)
139      FORMAT(' 0 0.0 0.0')
        TYPE 140,IB
140      FORMAT(10X,'NUMBER OF BUSSES IS....',I)
145      TYPE 150

```

```

*****
150      FORMAT(// ' NOW ENTER THE LOAD DATA IN THE FOLLOWING
MANNER;...
        1'/'(BUS  )(LOAD IN KVA)(PWR FACTOR)...OR...
        2'/'(BUS  )(LOAD IN HP)(PWR FACTOR)....OR....'/
        3'(BUS  )(LOAD IN AMPS)(PWR FACTOR)')
        DO 300 N=1,IB
            TYPE 160
160      FORMAT(' WHAT METHOD WILL YOU USE
?..VA,HP,OR AMPS??')
            ACCEPT 162,MD
162      FORMAT(A4)
            TYPE 164,MD
164      FORMAT(2X,A4,' ENTER...')
            IF(MD.EQ.'HP1') GO TO 170
            IF(MD.EQ.'HP') GO TO 170
            IF(MD.EQ.'AMPS') GO TO 180
            IF(MD.EQ.'S') GO TO 305
            MD='VA'
            ACCEPT 165, J,AS1,PFAC
165      FORMAT(I,2F)
            SZTZ=AS1/(ZBASE*1E3)
            SZR=SZTZ*PFAC
            PCOS=ACOS(PFAC)
            SZI=SZTZ*SIN(PCOS)
            S(J)=CMPLX(SZR,SZI)
            AI=AS1*1E3/(E(J)*SQRT(3.0))
            WRITE(33,168)J,AI
168      FORMAT(I,F)
            ST=MD
            GO TO 300
170      ACCEPT 175,I,PRH,PFAC
175      FORMAT(I,3F)
            SZTZ=PRH*746
            SZR=SZTZ*PFAC
            PCOS=ACOS(PFAC)
            SZI=SZTZ*SIN(PCOS)
            S(I)=CMPLX(SZR,SZI)/(ZBASE*1E6)
            IF(MD.EQ.'HP')XD(I)=.17/CABS(S(I))
            AI=SZTZ/(SQRT(3.0)*E(I))
            WRITE(33,178)I,AI
178      FORMAT(I,F)
            ST=MD
            GO TO 300
180      ACCEPT 185,I,CURT,PFAC
185      FORMAT(I,3F)
            WRITE(33,187)I,CURT
187      FORMAT(I,F)
            CURR=CURT*PFAC
            PCOS=ACOS(PFAC)
            CURI=CURT*SIN(PCOS)

```

```

CUR=CMPLX(CURR,CURI)
CUR=CUR*(SQRT(3.0)*EBASE/ZBASE)
S(I)=3*EBASE*CONJG(CUR)/SQRT(3.0)
ST=MD
300  CONTINUE
305  DO 320 N=1,IB
      NN=N
      TYPE 310,N,S(N),MD
310  FORMAT(' BUS ',I3,2F,A4,2F)
      WRITE(31,312)NN,S(NN)
312  FORMAT(I,2F)
      WRITE(32,315)N,S(N),XD(NN)
315  FORMAT(I,3F)
320  CONTINUE
      WRITE(31,330)
      WRITE(32,331)
330  FORMAT(' 0 0.0 0.0')
331  FORMAT(' 0 0.0 0.0')
      WRITE(33,332)
332  FORMAT(' 0 0.0')
      WRITE(35,335)
335  FORMAT(' 0 0 0.0 0.0 0.0 0.0 ')
      GO TO 900
400  OPEN(UNIT=36,FILE='RELA.DAT')
      READ(36,411) ZBASE,EBASE,IB
      IMAX=IB
411  FORMAT(2F,I)
450  READ(36,456)I,J,JJ,XL3,RES1,PU1,XL2,T1,S1
456  FORMAT(3I,9F)
      IF(I.EQ.0)GO TO 470
      L(I,J,JJ)=XL3
      RES(I,J,JJ)=RES1
      PU(I,J,1)=PU1
      XL(I,J,JJ)=XL2
      ZER(I,J,JJ)=CMPLX(0.0,XL2)
      ZG(I)=T1
      ZG(J)=S1
      IF(I.NE.0)GO TO 450
470  READ(36,472)I,E(I)
472  FORMAT(I,2F)
      IF(I.NE.0) GO TO 470
457  READ(36,458)I,S1
458  FORMAT(I,2F)
      S(I)=S1
      IF(I.NE.0) GO TO 457
      REWIND 36
      JJ=0
      CLOSE(UNIT=36)
      GO TO 12
900  CLOSE(UNIT=31)
      CLOSE(UNIT=32)

```

```

CLOSE(UNIT=35)
STOP
END
*****
C      LDFLO.F4:A LOAD FLOW PROGRAM
*****
      DIMENSION
E(33),Y1(33,33),PSCH(33),QSCH(33),PCAL(33),
1QCAL(33),PDIFF(33),QDIFF(33),IC(33),S(33),JAC(68,68)
,
      2PQVEC(33),EFDV(64),QQVEC(33),
      3YS(33,33),Y(33,33),CRFLO(33,33),U(68),V(68),
      4EDIFF(33)
      INTEGER P,Q,M,U,V,PP
      COMPLEX E,IC,Y,Z,YS,Y1,PFLO,PLOS,YSH,EDIFF,
      1S,CRFLO,PFLO1,ZG1,ZNI,ZNJ
      EQUIVALENCE (CRFLO,Y1)
      REAL JAC
      DIMENSION EIDV(64)

OPEN(UNIT=30,DEVICE='DSK',FILE='TEST.DAT',DISPOSE='SA
VE')
      OPEN(UNIT=33,DEVICE='DSK',FILE='DSK.XFR')
*****
CREAD VALUES OF IMPEDANCES  YSHUNT ADMITTANCES

C      888888*****IF SHUNT ADMITTANCES ARENOT IGNORED
REMOVE
***THE C IN THE LINE YS(Q,P)*****
C*****
      READ(30,2) IB,E1
2      FORMAT(I,F)
      E(1)=CMPLX(E1,0.0)
      DO 10 I=1,1000
      READ(30,5)NN,P,Q,JJ,Z,ZG1,ZNI,ZNJ
5      FORMAT(4I,8F)
      IF(P.EQ.0) GO TO 15
      YS(P,Q)=YSH
C      YS(Q,P)=YSH
      IF(CABS(Y1(P,Q)).NE.0)Z=1.0/(Y1(P,Q)+1/Z)
      Y1(P,Q)=1.0/Z
      Y1(Q,P)=Y1(P,Q)
      PRINT 6,P,Q,Y1(P,Q),YS(P,Q)
6      FORMAT(2I,4F)
10     CONTINUE
*****
CCOMPILE TERMS FOR YBUS
C*****
15     DO 50 P=1,1B
      Y(P,P)=0

```

```

DO 40 Q=1,IB
IF(P.EQ.Q) GO TO 40
Y(P,P)=Y(P,P)+Y1(P,Q)+YS(P,Q)
Y(P,Q)=-Y1(P,Q)
40 CONTINUE
50 CONTINUE
C*****
C PRINT OUT VALUES OF YBUS
C*****
PRINT 51
51 FORMAT ('0',10X,'BUS IMPEDANCE MATRIX,YBUS')
DO 58 I=1,IB
PRINT 54,(Y(I,J),J=1,IB)
54 FORMAT('0',100F)
58 CONTINUE
C*****
C READ VALUES OF POWER AT BUSES
C*****
DO 60 P=1,IB
READ(30,59) I,PS,QS
IF(I.EQ.0)GO TO 62
IF(I.EQ.1)GO TO 60
PSCH(I)=-PS
QSCH(I)=-QS
59 FORMAT(I,2F)
60 CONTINUE
C*****
C ASSUME VALUES OF VOLTAGE AT BUSES
C*****
62 DO 70 P=2,IB
E(P)=(1.0,0.0)
70 CONTINUE
K=0
DO 80 I=1,IB
TYPE 75,I,E(I)
75 FORMAT(I,2F)
80 CONTINUE
122 PRINT 123,K
123 FORMAT ('0',85X,'ITERATION = ',I2)
C*****
C CALCULATES REAL REACTIVE BUSS POWERS
C*****
DO 150 P=2,IB
PSUM=0
QSUM=0
DO 140 Q=1,IB

P1=REAL(E(P))*(REAL(E(Q))*REAL(Y(P,Q))-AIMAG(E(Q))*AI
MAG(Y
I(P,Q)))+AIMAG(E(P))*(AIMAG(E(Q))*REAL(Y(P,Q))+REAL(E

```

```

(Q))*
      2AIMAG(Y(P,Q)))

Q1=AIMAG(E(P))*(REAL(E(Q))*REAL(Y(P,Q))-AIMAG(E(Q))*A
IMAG(Y

1(P,Q)))-REAL(E(P))*(AIMAG(E(Q))*REAL(Y(P,Q))+REAL(E(
Q))*AI
      2MAG(Y(P,Q)))
      PSUM=PSUM+P1
      QSUM=QSUM+Q1
140      CONTINUE
      PCAL(P)=PSUM
      QCAL(P)=QSUM
      PRINT 145,PCAL(P),QCAL(P)
145      FORMAT(2F)
150      CONTINUE
C*****
C PRINT OUT VALUES OF CALCULATED BUSS POWERS
C*****
      PRINT 155,K
155      FORMAT('0','REAL AND REACTIVE BUSS POWERS K=',I2)
      DO 158 I=2,IB
      PRINT 157,PCAL(I),QCAL(I)
157      FORMAT ('0',2F)
158      CONTINUE
      M=0
      DO 160 P=2,IB
      EP=0.01
      PDIFF(P)=PSCH(P)-PCAL(P)
      QDIFF(P)=QSCH(P)-QCAL(P)
      TDIFF=ABS(PDIFF(P))+ABS(QDIFF(P))
      IF(TDIFF.LT.EP) GO TO 160
      M=1
160      CONTINUE
C*****
C PRINT OUT VALUES OF DIFFERENTIAL BUSS POWERS
C*****
      PRINT 165,K
165      FORMAT('0','DIFFERENTIAL PQ      K=',3X,I2)

      DO 168 I=2,IB
      PRINT 167,PDIFF(I),QDIFF(I)
167      FORMAT ('0',2F)
168      CONTINUE
      IF(M.EQ.0) GO TO 400
      DO 170 I=2,IB
      S(I)=CMPLX(PCAL(I),QCAL(I))
170      CONTINUE
C*****
C CALCULATE BUSS CURRENTS I(P) EXCEPT AT SLACK BUS

```

```

C*****
      DO 175 I=2,IB
      IC(I)=CONJG(S(I))/CONJG(E(I))
      PRINT 173,IC(I)
173      FORMAT(F)
175      CONTINUE
C*****
C  CALCULATE JACOBIAN USING PARTITIONS 'J1,J2,J3,J4'
C*****
C  JACOBIAN 'J1'
C*****
      IBDJ=2*IB-2
      IBJ=IB-1
      DO 190 M=1,IBJ
      DO 180 N=1,IBJ
      P=M+1
      Q=N+1

JAC(M,N)=(REAL(E(P))*REAL(Y(P,Q)))+(AIMAG(E(P))*AIMAG
(Y(P,Q)))
      IF(P.NE.Q) GO TO 177
      JAC(M,N)=JAC(M,N)+REAL(IC(P))
177      CONTINUE
C      PRINT 178,JAC(M,N),E(P),Y(P,Q)
178      FORMAT(5F)
180      CONTINUE
190      CONTINUE
*****
C  JACOBIAN 'J2'
*****
      DO 210 M=1,IBJ
      DO 200 N=IB,IBDJ
      P=M+1
      Q=N-IB+2

JAC(M,N)=-REAL(E(P))*AIMAG(Y(P,Q))+AIMAG(E(P))*REAL(Y
(P,Q))
      IF(P.NE.Q) GO TO 195
      JAC(M,N)=JAC(M,N)+AIMAG(IC(P))
195      CONTINUE
200      CONTINUE
210      CONTINUE
*****
C  JACOBIAN 'J3'
*****
      DO 230 M=IB,IBDJ
      DO 220 N=1,IBJ
      P=M-IB+2
      Q=N+1

JAC(M,N)=-REAL(E(P))*AIMAG(Y(P,Q))+AIMAG(E(P))*REAL(Y

```

```

(P,Q))
      IF(P.NE.Q) GO TO 215
      JAC(M,N)=JAC(M,N)-AIMAG(IC(P))
215    CONTINUE
220    CONTINUE
230    CONTINUE
*****
C  JACOBIAN 'J4'
*****
      DO 250 M=IB,IBDJ
      DO 240 N=IB,IBDJ
      P=M-IB+2
      Q=N-IB+2

JAC(M,N)=-AIMAG(E(P))*AIMAG(Y(P,Q))-REAL(E(P))*REAL(Y
(P,Q))
      IF(P.NE.Q) GO TO 235
      JAC(M,N)=JAC(M,N)+REAL(IC(P))
235    CONTINUE
240    CONTINUE
250    CONTINUE
      DO 334 M=1,IBDJ
C      PRINT 333,(JAC(M,N),N=1,IBDJ)
333    FORMAT(18F)
334    CONTINUE
*****
*****
C  COMPUTE INVERSE OF JACOBIAN
      CALL MINV(JAC,68,IBDJ)
*****
C      PRINT 344,(JAC(M,N),N=1,IBDJ)
344    FORMAT(18F)
345    CONTINUE
*****
C  COMPUTE DIFFERENCE IN VOLTAGE USING JACOBIAN INVERSE 'JAC'
*****
      DO 346 I=2,IB
      M=I-1
      PQVEC(M)=PDIFF(I)
      QQVEC(M)=QDIFF(I)
346    CONTINUE
      J=IB-1
      DO 351 M=1,J
      EFDVD=0
      EFDQD=0
      EIDD=0
      EIQV=0
      DO 349 N=1,J
      EFDVD=EFDVD+JAC(M,N)*PQVEC(N)
349    CONTINUE
      DO 350 N=IB,IBDJ

```



```

      NQ=N-J
      EFDQD=EFDQD+JAC(M,N)*QQVEC(NQ)
350      CONTINUE
      EFDV(M)=EFDQD+EFDVD
351      CONTINUE
      DO 360 M=IB,IBDJ
      EIDD=0
      EIQV=0
      DO 358 N=1,J
      EIDD=EIDD+JAC(M,N)*PQVEC(N)
358      CONTINUE
      DO 359 N=IB,IBDJ
      NQ=N-J
      EIQV=EIQV+JAC(M,N)*QQVEC(NQ)
359      CONTINUE
      EIDV(M)=EIQV+EIDD
360      CONTINUE
*****
C   COMPUTE NEW BUS VOLTAGES USING 'EFDV' EFDIFFERENTIAL
VECTOR
*****
      DO 370 P=2,IB
      M=P-1
      N=M+J
      IBZ=2*(IB-1)
      IF(N.GT.IBZ) GO TO 370
      EDIFF(P)=CMPLX(EFDV(M),EIDV(N))
      PRINT 368,P,EDIFF(P)
368      FORMAT(I,2F)
      E(P)=E(P)+EDIFF(P)
370      CONTINUE
      IF(K.EQ.10)GO TO 390
      K=K+1
      GO TO 122
390      TYPE 395
395      FORMAT(' AN ERROR IS MADE IN DATA, LOAD FLOW DID NOT
CONVERGE')
400      CONTINUE
500      CLOSE(UNIT=30)
*****
C   COMPUTE POWER FLOWS BUS P TO Q
C   COMPUTE CURRENT FLOWS AND POWER LOSSES
C   COMPUTE SLACK BUS POWER
*****
      OPEN(UNIT=31,FILE='DSK')
      S(1)=0
503      FORMAT(I)
      DO 520 P=1,IB
      DO 515 Q=1,IB
      IF(P.EQ.Q) GO TO 515
      IF(Y(P,Q).EQ.(0.0,0.0)) GO TO 515

```

```

      PP=P
*****
C      IF YOU ARE NOT NEGLECT SHUNT ADMITT REMOVE THE NEXT
C
*****
      PFLO=CONJG(E(P))*((E(P)-E(Q))*Y1(P,Q))
C      1+(CONJG(E(P))*E(P)*YS(P,Q))
      PFLO1=CONJG(E(Q))*((E(Q)-E(P))*Y1(P,Q))
C      1+(CONJG(E(Q))*E(Q)*YS(P,Q))
      CRFLO(P,Q)=PFLO/CONJG(E(P))
      PLOS=PFLO+PFLO1
*****
C      TAKE THE CONJUGATE OF THE POWER FLOWS FOR FORMAT
P-JQ
*****
      PLOS=CONJG(PLOS)
      PFLO=CONJG(PFLO)
      IF(P.NE.1) GO TO 505
      S(1)=PFLO+S(1)
505    WRITE(31,509)P,Q,PFLO,CRFLO(P,Q),PLOS
      WRITE(31,510)PP,E(PP)
509    FORMAT(6X,'POWER FLOW
BUS',I2,'TO',I2,'IS',2F,2X,'CURRENT
      1FLOW IS',2F,'POWER LOSS IS',2F)
510    FORMAT(5X,'BUS',I2,'VOLTAGE IS',2F)
515    CONTINUE
520    CONTINUE
      WRITE(31,540) S(1)
540    FORMAT(6X,'POWER AT SLACK BUS 1 IS',2F)
      DO 550 M=1,IB
          DO 545 N=1,IB
              IF(CABS(CRFLO(M,N)).GT.0.000001)
WRITE(33,543)M,N,
          1CRFLO(M,N)
543    FORMAT(2I,2F)
545    CONTINUE
550    CONTINUE
      WRITE(33,555)
555    FORMAT(' 0 0 0.0 0.0')
      CLOSE(UNIT=33)
      DO 600 M=1,IB
          DO 580 N=1,IB
              S(2)=E(M)*CONJG(CRFLO(M,N))
              PFAD=CABS(S(2))
              IF(PFAD.EQ.0) GO TO 580
              PFAC=-(REAL(S(2)))/(PFAD)
              WRITE(31,570)M,N,PFAC
570    FORMAT(4X,'POWER FACTOR BUS',I3,'TO',I3,'IS',F)
580    CONTINUE
600    CONTINUE
      CLOSE(UNIT=31)

```

```

      STOP
      END
C     TITLE:MINV;SUBROUTINE TO INVERT A REAL SQUARE MATRIX
      SUBROUTINE MINV(A,MDIM,N)
      DIMENSION A(MDIM,N)
      INTEGER L(100),M(100)

C
C     CONVERTED FROM SSP ROUTNE MINV
C
      DO 80 K=1,N
      L(K)=K
      M(K)=K
      BIGA=A(K,K)
      DO 20 J=K,N
      DO 20 I=K,N
10     IF(ABS(BIGA)-ABS(A(I,J))) 15,20,20
15     BIGA=A(I,J)
      L(K)=I
      M(K)=J
20     CONTINUE
      J=L(K)
      IF(J-K) 35,35,25
25     DO 30 I=1,N
      HOLD=-A(K,I)
      A(K,I)=A(J,I)
30     A(J,I)=HOLD
35     I=M(K)
      IF(I-K) 45,45,38
38     DO 40 J=1,N
      HOLD=-A(J,K)
      A(J,K)=A(J,I)
40     A(J,I)=HOLD
45     DO 55 I=1,N
      IF(I-K) 50,55,50
50     A(I,K)=A(I,K)/(-BIGA)
55     CONTINUE
      DO 65 I=1,N
      HOLD=A(I,K)
      DO 65 J=1,N
      IF(I-K) 60,65,60
60     IF(J-K) 62,65,62
62     A(I,J)=HOLD*A(K,J)+A(I,J)
65     CONTINUE
      DO 75 J=1,N
      IF(J-K) 70,75,70
70     A(K,J)=A(K,J)/BIGA
75     CONTINUE
      A(K,K)=(1.0000000)/BIGA
80     CONTINUE
      K=N
100    K=K-1

```

```

      IF(K) 150,150,105
105      I=L(K)
      IF(I-K) 120,120,108
108      DO 110 J=1,N
          HOLD=A(J,K)
          A(J,K)=-A(J,I)
110      A(J,I)=HOLD
120      J=M(K)
          IF(J-K) 100,100,125
125      DO 130 I=1,N
          HOLD=A(K,I)
          A(K,I)=-A(J,I)
130      A(J,I)=HOLD
          GO TO 100
150      RETURN
      END

```

```

*****
C      TITLE:ZBUS.F4;ACCEPTS DATA FROM TEST.DAT AND DSK.XFR
FROM
C      LOAD FLOW PROGRAM LDFLO.F4 AND FORMS ZBUS BY
C      ALGORITHM THIS WILL BE USED TO COMPUTE ALL
FAULT
C      CURRENTS.LOAD FLOW COMPUTED MAXIMUM LOAD
CURRENTS.

```

```

*****
*****
C      READ DATA FROM TEST.DAT
*****

```

```

      DIMENSION
ZD(300,3),ZM(300,2),RID(30,30,3),ZG(30),ZN(30),
1ID(200),RI(30),ZB(30,30),ZBO(30,30),ZMU(5,5),IDD(5),
ZL(30),

```

```

      2ZBR(30),ZGO(30),ZLO(30),EB(30)
      COMPLEX ZD,ZM,ZG,T1,ZN,ZN1,ZNI,ZNJ,ZG1,ZO,
      1ZB,ZBO,ZMU,ZBB,ZL,ZLL,ZBR,ZGO,ZLO,ZLLO,EB
      NNB=1
      EQUIVALENCE(ZBR,ZLO,EB)
      OPEN(UNIT=31,FILE='TEST.DAT')
C      OPEN(UNIT=32,FILE='DSK.XFR')
      READ(31,10)IB,EB1
10      FORMAT(I,F)
20      READ(31,30)NB,I,J,JJ,T1,ZG1,ZNI,ZNJ
30      FORMAT(4I,8F)
      IF(NB.EQ.0) GO TO 40
      DN=NB
      NN=NB
      ZD(NN,1)=CMPLX(DN,0.0)
      ZD(NN,2)=T1
      ZD(NN,3)=ZG1+3*ZN(I)
      ZN(I)=ZNI

```

```

ZN(J)=ZNJ
RID(I,J,JJ)=NN
IF(NB.NE.0)GO TO 20
40  DO 45 I=1,IB
C    READ(32,43)T1
43    FORMAT(2F)
45    CONTINUE
      DO 48 I=1,IB
C    READ(32,46)J,T1
46    FORMAT(1,2F)
      EB(J)=T1
48    CONTINUE
49    READ(31,50)I,T1,XD1
50    FORMAT(1,3F)
      IF(I.EQ.0) GO TO 60
      IF(CABS(T1).EQ.0) GO TO 49
C    T1=CONJG(T1)
C    ZG(I)=3*(CABS(EB(I))*2)/T1
      IF(XD1.NE.0)ZG(I)=CMPLX(0.0,XD1)
      ZG(I)=ZG(I)
      IF(I.NE.0) GO TO 49
*****
C    ENTER THE ZERO SEQ IMP BUS TO REF(GROUND)
*****
60    TYPE 62
62    FORMAT(' ENTER THE SYNC ZERO SEQUENCE IMPEDENCE FOR
THE LOADS
      1AT EACH'/' BUS,3*ZN,MUST BE ADDED,IMPED IN PU.,')
      DO 65 I=1,IB
      ACCEPT 64,II,T1
      IF(II.EQ.0)GO TO 66
      ZG(II)=T1
64    FORMAT(1,2F)
65    CONTINUE
66    DO 68 I=1,IB
      IF(CABS(ZG(I)).EQ.0)ZG(I)=ZG(I)
68    CONTINUE
*****
C    ENTER THE MUTUALLY COUPLED ELEMENTS
*****
      CLOSE(UNIT=31)
      TYPE 70
70    FORMAT(' ENTER THE MUTUALLY COUPLED ELEMENTS IN PER
UNIT'/'
      1 IN THE FOLLOWING FORMAT,TEST.DAT HAS THE ELEMENT
      S.,'/'
      2 (ELEMENT )SP TO(ELEMENT )SP(0 SEQ VALUE) ')
75    ACCEPT 80,EL,ELL,ZO
80    FORMAT(4F)
      IF(EL.EQ.0.0) GO TO 100
      II=II+1

```

```

      ZM(II,1)=CMPLX(EL,ELL)
      ZM(II,2)=Z0
      GO TO 75
*****
C      ALL ELEMENT DATA PREPARED PERFORM POSITIVE AND
NEGATIVE
C      SEQUENCE COMPUTATIONS TO FORM ZBUS
*****
*****
100      DO 500 IEL=1,NN
          BRA=0
          ID(IEL)=1
          DO 120 I=1,30
              DO 120 J=1,30
                  DO 120 JJ=1,3
                      IF(RID(I,J,JJ).NE.IEL) GO TO
120
110
115
110
115
115
120
181
186
190
195
          IF(RI(I).EQ.0)GO TO
          IF(RI(J).EQ.0)GO TO
          BRA=1.0
          IPP=MINO(I,J)
          IQQ=MAXO(I,J)
          GO TO 130
          IF(RI(J).EQ.0)GO TO
          RI(I)=1.0
          IPP=J
          IQQ=I
          GO TO 130
          RI(J)=1.0
          RI(I)=1.0
          IPP=MINO(I,J)
          IQQ=MAXO(I,J)
          GO TO 130
          CONTINUE
*****
C      BRANCH OR LINK HAS BEEN DETERMINED BRA=0:BRANCH
*****
130      DO 195 IL=1,IB
          ZBB=CMPLX(0.0,0.0)
          IF(BRA.NE.0) GO TO 136
          IF(IQQ.EQ.IL) GO TO 190
          ZBR(IL)=ZB(IPP,IL)
          GO TO 190
          ZL(IL)=ZB(IPP,IL)-ZB(IQQ,IL)
          CONTINUE
          CONTINUE
          ZBB=CMPLX(0.0,0.0)
          IF(BRA.NE.0) GO TO 250

```



```

615 IF(RI(J).EQ.0) GO TO 625
    BRA=1.0
    IPP=MINO(I,J)
    IQQ=MAXO(I,J)
    GO TO 625
610 IF(RI(J).EQ.0) GO TO 625
615 RI(I)=1.0
    IPP=J
    IQQ=I
    GO TO 625
615 RI(I)=1.0
    RI(J)=1.0
    IPP=I
    IQQ=J
    GO TO 625
620 CONTINUE
*****
C SEARCH FOR MUTUAL COUPLING IN ZERO SEQUENCE
*****
625 IDD(1)=IEL
    DO 650 I=1,NN
        DM=IEL
        IF(REAL(ZM(I,1)).EQ.DM)MUT=1
        IF(AIMAG(ZM(I,1)).EQ.DM)MUT=1
        IF(MUT.NE.1)GO TO 650
        MUT=0
        I11=IFIX(REAL(ZM(I,1)))
        I12=IFIX(AIMAG(ZM(I,1)))
        IF(ID(I11).EQ.0)GO TO 650
        IF(ID(I12).EQ.0)GO TO 650
        IF(I11.EQ.IEL)GO TO 630
        I13=I11
        I11=I12
        I12=I13
630 IDD(1)=I11
        NNB=NNB+1
        IDD(NNB)=I12
        DM=I12
        DO 645 J1=1,NN
            IF(REAL(ZM(J1,1)).EQ.DM)MUT=1
            IF(AIMAG(ZM(J1,1)).EQ.DM)MUT=
1
                IF(MUT.NE.1) GO TO 645
                MUT=0
                I111=IFIX(REAL(ZM(J1,1)))
                I112=IFIX(AIMAG(ZM(J1,1)))
                IF(ID(I111).EQ.0)GO TO 645

```



```

IF(ID(III2).EQ.0)GO TO 645
IF(III1.EQ.DM) GO TO 643
III3=III1
III1=III2
III2=III1
643 IF(III2.EQ.III1) GO TO 645
NNB=NNB+1
IDD(NNB)=III2
645 CONTINUE
650 CONTINUE
DO 660 I=1,NNB
ZMU(I,I)=ZD(IDD(I),3)
DO 660 J=1,NNB
DD1=IDD(I)
DD2=IDD(J)
DO 660 KK=1,NN

IF(ZM(KK,1).EQ.CMPLX(
DD1,DD2))
1MUT=1

IF(ZM(KK,1).EQ.CMPLX(DD2,DD1)
) MUT=1

IF(MUT.NE.1)GO TO 660
MUT=0
ZMU(I,J)=ZM(KK,2)
ZMU(J,I)=ZM(KK,2)

660 CONTINUE
*****
C ZMU IS FORMED
*****
DO 665 I=1,NNB
DO 665 J=1,NNB
PRINT 663,I,J,ZMU(I,J)
663 FORMAT(2I,2F)
665 CONTINUE
*****
CALL CMXINV(ZMU,5,NNB)
*****
DO 668 I=1,NNB
PRINT 667,(ZMU(I,J),J=1,NNB)
667 FORMAT(10F)
668 CONTINUE
DO 695 IL=1,IB
IF(NNB.EQ.1) GO TO 681
ZBB=CMPLX(0.0,0.0)
DO 680 J4=1,NNB
J=J4+1
I=IDD(J)
IF(I.EQ.0) GO TO 630
DO 670 I1=1,30

```

DO 670 I2=1,30  
DO 670

I3=1,3

IF(RI  
D(I1,I2,I3  
1).NE.I)GO TO 670

IP=I1

IQ=I2

ZBB=(ZMU(1,J)/ZMU(1,1))\*(ZBO(IP,IL)-ZBO(IQ,IL))+ZBB

670

CONTINUE

680

CONTINUE

681

IF(BRA.NE.0) GO TO 686

IF(IQQ.EQ.IL) GO TO 690

ZBR(IL)=ZBO(IPP,IL)+ZBB

GO TO 690

686

ZL(IL)=ZBB+ZBO(IPP,IL)-ZBO(IQQ,IL)

690

CONTINUE

695

CONTINUE

ZBB=CMPLX(0.0,0.0)

IF(BRA.NE.0) GO TO 750

DO 700 IL=1,IB

ZBO(IQQ,IL)=ZBR(IL)

ZBO(IL,IQQ)=ZBR(IL)

700

CONTINUE

IF(NNB.EQ.1) GO TO 740

DO 730 J=2,NNB

I=IDD(J)

DO 720 I1=1,30

DO 720 I2=1,30

DO 720 I3=1,3

IF(RID(I1,I2,I3).NE.I) GO TO 720

IP=I1

IQ=I2

720

CONTINUE

ZBB=(ZMU(1,J)\*(ZBO(IP,IQQ)-ZBO(IQ,IQQ  
))/  
1ZMU(1,1))+ZBB

730

CONTINUE

740

ZBO(IQQ,IQQ)=ZBO(IPP,IQQ)+ZBB+1.0/ZMU(1,1)

ZBB=CMPLX(0.0,0.0)

GO TO 800

750

IF(NNB.EQ.1) GO TO 781

DO 780 J=2,NNB

I=IDD(J)

DO 770 I1=1,30

DO 770 I2=1,30

DO 770 I3=1,3

```

112,I3).NE.I)GO TO 770
IF(RID(I1,
IP=I1
IQ=I2

770          CONTINUE

ZBB=(ZMU(I,J)*(ZL(IP)-ZL(IQ))/ZMU(1,1
))+ZBB
780          CONTINUE
781          ZLL=ZL(IPP)-ZL(IQQ)+ZBB+(1.0/ZMU(1,1))
          ZBB=CMPLX(0.0,0.0)
          DO 790 IP=1,IB
          DO 790 IQ=1,IB
          IF(IP.GT.IQ)GO TO 790

ZB0(IP,IQ)=ZB0(IP,IQ)-(ZL(IP)
*ZL(IQ)
          1/ZLL)
          IF(IP.EQ.IQ) GO TO 790
          ZB0(IQ,IP)=ZB0(IP,IQ)

790          CONTINUE
800          DO 850 I=1,5
          DO 850 J=1,5
          ZMU(I,J)=CMPLX(0.0,0.0)
          IDO(I)=0

850          CONTINUE
          DO 900 I=1,IB
          DO 900 J=1,IB
          PRINT 880,I,J,ZB0(I,J)
          FORMAT(2I,2F)

880          CONTINUE
900          NNB=1

1000         CONTINUE
*****
C          ZBUS ZERO IS FORMED
*****
          OPEN(UNIT=33,FILE='ZBUS.FOR')
          DO 1010 I=1,IB
          DO 1010 J=1,IB
          WRITE(33,1005)I,J,ZB0(I,J),ZB(I,J),ZB(I,J)
1005         FORMAT(2I,6F)
          PRINT 1007
1007         FORMAT(3X,'BUS TO BUS ',3X,'ZERO SEQ ',5X,'POS
SEQ')
          PRINT 1008,I,J,ZB0(I,J),ZB(I,J)
1008         FORMAT(2I6,4F)
1010         CONTINUE
          CLOSE(UNIT=32)
*****
C          NOW TO ADD ALL LOADS. ALL LOADS WILL BE LINKS WITH

```

```

NO
C      MUTUAL COUPLING.
*****
DO 1200 I=1,IB
      IF(CABS(ZG(I)).EQ.0)GO TO 1200
DO 1100 IL=1,IB
      ZL(IL)=-ZB(I,IL)
      ZLO(IL)=-ZBO(I,IL)
1100      CONTINUE
      ZLL=-ZL(I)+ZG(I)
      ZLLO=-ZLO(I)+ZGO(I)
DO 1150 J=1,IB
      DO 1150 K=1,IB
          IF(J.GT.K)GO TO 1150

ZB(J,K)=ZB(J,K)-ZL(J)*ZL(K)/Z
LL
                                ZB(K,J)=ZB(J,K)

ZBO(J,K)=ZBO(J,K)-ZLO(J)*ZLO(
K)/ZLLO
                                ZBO(K,J)=ZBO(J,K)
1150      CONTINUE
1200      CONTINUE
      OPEN(UNIT=34,FILE='ZBUS.DAT')
DO 1300 I=1,IB
      DO 1300 J=1,IB
WRITE(34,1250)I,J,ZB(I,J),ZBO(I,J)
1250      FORMAT(2I,4F)
1300      CONTINUE
      CLOSE(UNIT=34)
      CLOSE(UNIT=33)
      OPEN(UNIT=36,FILE='MUT.CO')
DO 1400 I=1,NN
      EL1=REAL(ZM(I,1))
      IF(EL1.EQ.0.0)GO TO 1322
      EL2=AIMAG(ZM(I,1))
      IEL1=IFIX(EL1)
      IEL2=IFIX(EL2)
DO 1320 I1=1,IB
DO 1320 J1=1,IB
DO 1320 K1=1,IB
      IF(RID(I1,J1,K1).EQ.EL1)GO TO 1310
      IF(RID(I1,J1,K1).EQ.EL2)GO TO 1315
GO TO 1320
1310      IBII=I1
      IBIJ=J1
GO TO 1320
1315      IBJI=I1
      IBJJ=J1
1320      CONTINUE

```

```

1322     IF(EL1.EQ.0)GO TO 1400

WRITE(36,1350)EL1,EL2,IBII,IBIJ,IBJI,IBJJ,ZM(
I,2)
1350             FORMAT(2F,4I3,2F)
1400     CONTINUE
        WRITE(36,1450)
1450     FORMAT('  0.0 0.0 0 0 0 0 0.0 0.0')
        CLOSE(UNIT=36)
        STOP
        END

C      TITLE:CMXINV;SUBROUTINE FOR INVERT COMPLEX MATRIX
        SUBROUTINE CMXINV(A,MDIM,N)
        COMPLEX A(MDIM,N),BIGA,HOLD
        INTEGER L(100),M(100)

C
C      CONVERTED FROM SSP ROUTNE MINV
C
        DO 80 K=1,N
        L(K)=K
        M(K)=K
        BIGA=A(K,K)
        DO 20 J=K,N
        DO 20 I=K,N
10      IF(CABS(BIGA)-CABS(A(I,J))) 15,20,20
15      BIGA=A(I,J)
        L(K)=I
        M(K)=J
20      CONTINUE
        J=L(K)
        IF(J-K) 35,35,25
25      DO 30 I=1,N
        HOLD=-A(K,I)
        A(K,I)=A(J,I)
30      A(J,I)=HOLD
35      I=M(K)
        IF(I-K) 45,45,38
38      DO 40 J=1,N
        HOLD=-A(J,K)
        A(J,K)=A(J,I)
40      A(J,I)=HOLD
45      DO 55 I=1,N
        IF(I-K) 50,55,50
50      A(I,K)=A(I,K)/(-BIGA)
55      CONTINUE
        DO 65 I=1,N
        HOLD=A(I,K)
        DO 65 J=1,N
        IF(I-K) 60,65,60
60      IF(J-K) 62,65,62
62      A(I,J)=HOLD*A(K,J)+A(I,J)

```

```

65      CONTINUE
        DO 75 J=1,N
          IF(J-K) 70,75,70
70      A(K,J)=A(K,J)/BIGA
75      CONTINUE
          A(K,K)=(1.0000000,0.0000000)/BIGA
80      CONTINUE
          K=N
100     K=K-1
          IF(K) 150,150,105
105     I=L(K)
          IF(I-K) 120,120,108
108     DO 110 J=1,N
          HOLD=A(J,K)
          A(J,K)=-A(J,I)
110     A(J,I)=HOLD
120     J=M(K)
          IF(J-K) 100,100,125
125     DO 130 I=1,N
          HOLD=A(K,I)
          A(K,I)=-A(J,I)
130     A(J,I)=HOLD
          GO TO 100
150     RETURN
        END

```

```

*****
C      TITLE:FALT.F4;TAKES DATA FROM ZBUS.DAT AND COMPUTES
C      ALL FAULT CURRENTS AT ALL BUSES
*****

```

```

      DIMENSION
ZB(30,30),ZB0(30,30),FCUR(300,3,2),EFALT(30,3,2)
      1,EB(30),IDELE(300),EIB(30)
      COMPLEX
ZB,ZB0,FCUR,EFALT,EB,EB1,ZB1,ZB01,ZR1,ZN1,ZNI,ZNJ,
      1ZR2,ZN2,ZF,IDELE,FCUR1,FCUR2,ALCUR
      OPEN(UNIT=34,FILE='TEST.DAT')
      OPEN(UNIT=35,FILE='ZBUS.DAT')
      READ(34,5) IB,E1
5      FORMAT(1,F)
      IBB=IB*IB
      DO 7 I=1,IB
      EB(I)=CMPLX(E1,0.0)
7      CONTINUE
9      READ(34,10),NI,I,J,K
10     FORMAT(4I)
      IF(NI.EQ.0)GO TO 15
      IF(K.EQ.2)I=-I
      IF(K.EQ.3)J=-J
      RI=I
      RJ=J
      IDELE(NI)=CMPLX(RI,RJ)

```

```

      IF(NI.NE.0)GO TO 9
15      DO 30 II=1,IBB
      READ(35,25)I,J,ZB1,ZB01
25      FORMAT(2I,4F)
      ZB(I,J)=ZB1
      ZB0(I,J)=ZB01
30      CONTINUE
      CLOSE(UNIT=35)
      OPEN(UNIT=37,FILE='MUT.CO')
      OPEN(UNIT=38,FILE='FALT.DAT')
      OPEN(UNIT=39,FILE='EFLT.DAT')
      OPEN(UNIT=40,FILE='RELA.DAT')
      OPEN(UNIT=41,FILE='FCUR.DAT')
      OPEN(UNIT=42,FILE='DSK.XFR')
      OPEN(UNIT=43,FILE='LCUR.DAT')
      READ(40,32) RMVAB,RKVBA,IRR
32      FORMAT(2F,I)
      RKVBA=RKVBA*1E3
      FIPU=RMVAB*1E6/((SQRT(3.0)*RKVBA)
33      READ(40,34)IRR
34      FORMAT(I)
      IF(IRR.NE.0)GO TO 33
36      READ(40,37)J,E
37      FORMAT(I,F)
      IF(J.EQ.0)GO TO 38
      EIB(J)=E
      GO TO 36
38      TYPE 35
35      FORMAT(' ENTER THE FAULT
IMPEDENCE-REAL(SP)IMAGINARY...')
      ACCEPT 40,ZF
40      FORMAT(2F)
      DO 500 IFLT=1,IB
      IF(CABS(ZB(IFLT,IFLT)).EQ.0)GO TO 500
      DO 50 I=1,IB
      IF(I.EQ.IFLT)GO TO 45

EFALT(I,2,1)=SQRT(3.0)*(EB(I)-((ZB(I,
IFLT)*EB
      1(IFLT))/(ZF+ZB(IFLT,IFLT))))

EFALT(I,1,2)=-((SQRT(3.0)*EB(IFLT)*ZB0
(I,IFLT)/
      1(ZB0(IFLT,IFLT)+3*ZF+(2*ZB(IFLT,IFLT))))

EFALT(I,2,2)=SQRT(3.0)*EB(I)-((SQRT(3
.0)*EB
      1(IFLT)*ZB(I,IFLT))/(ZB0(IFLT,IFLT)+(2*(ZB(IFLT,IFLT)
)+3*ZF)))

```

```
EFALT(I,3,2)=EFALT(I,2,2)-(SQRT(3.0)*
EB(I))
```

```
GO TO 50
```

```
45
```

```
EFALT(IFLT,2,1)=SQRT(3.0)*(ZF*EB(IFLT
)/(ZF+
1ZB(IFLT,IFLT)))
```

```
EFALT(IFLT,1,2)=-SQRT(3.0)*EB(IFLT)*Z
BO(IFLT,
1IFLT)/(ZBO(IFLT,IFLT)+(2*ZB(IFLT,IFLT))+3*ZF)
```

```
EFALT(IFLT,2,2)=SQRT(3.0)*EB(IFLT)*(Z
BO(IFLT,
1IFLT)+ZB(IFLT,IFLT)+3*ZF)/(ZBO(IFLT,IFLT)+(2*ZB(IFLT
,IFLT))+3*
2ZF)
```

```
EFALT(IFLT,3,2)=-SQRT(3.0)*EB(IFLT)*Z
B(IFLT,IFL
1T)/(ZBO(IFLT,IFLT)+(2*ZB(IFLT,IFLT))+3*ZF)
```

```
50
```

```
CONTINUE
REWIND 34
REWIND 37
```

```
WRITE(39,53)(IFLT,I,EFALT(I,2,1),EFALT(I,1,2)
```

```
,
1EFALT(I,2,2),EFALT(I,3,2),I=1,IB)
```

```
53 FORMAT(2I3,8F)
```

```
READ(34,55)II,E
```

```
55 FORMAT(1,F)
```

```
DO 90 K=1,IBB
```

```
READ(34,60)NN,I,J,KK,ZR1,ZN1,ZNI,ZNJ
```

```
60 FORMAT(4I,8F)
```

```
IF(NN.EQ.0)GO TO 91
```

```
FCUR(NN,2,1)=(EFALT(I,2,1)-EFALT(J,2,1))/ZR1
```

```
FCUR(NN,1,2)=(EFALT(I,1,2)-EFALT(J,1,2))/(ZN1
+3*
```

```
1(ZNI+ZNJ))
```

```
FCUR(NN,2,2)=(EFALT(I,2,2)-EFALT(J,2,2))/ZR1
```

```
FCUR(NN,3,2)=(EFALT(I,3,2)-EFALT(J,3,2))/ZR1
```

```
DO 85 I2=1,IBB
```

```
READ(37,65)RN1,RN2,IBII,IBIJ,
IBJI,IBJJ
```

```
1,ZN2
```

```
65
```

```
FORMAT(2F,4I,2F)
```

```
NN1=IFIX(RN1)
```

```
NN2=IFIX(RN2)
```



```

IF(NN1.EQ.NN)GO TO 70
IF(NN2.EQ.NN) GO TO 74
IF(NN1.EQ.0)GO TO 86
GO TO 85
70    FCUR(NN,1,2)=((EFALT(IBJ1,1,2)-EFALT(IBJJ,1,2))/
1(ZN2))+FCUR(NN,1,2)
GO TO 85
74    FCUR(NN,1,2)=((EFALT(IBI1,1,2)-EFALT(IBIJ,1,2))/
1(ZN2))+FCUR(NN,1,2)
85    CONTINUE
86    REWIND 37
90    CONTINUE
91    REWIND 34
DO 300 NN=1,IBB
IF(CABS(FCUR(NN,2,1)).EQ.0)GO TO 300

WRITE(38,250)IFLT,NN,FCUR(NN,2,1),FCU
R(NN,1,2)
1,FCUR(NN,2,2),FCUR(NN,3,2)
250    FORMAT(2I3,8F)
300    CONTINUE
DO 400 NN=1,IBB
IF(CABS(FCUR(NN,2,1)).EQ.0)GO TO 400

FCUR1=(RKVBA/EIB(IFIX(ABS(REAL(IDELE(
NN)
1)))))*FCUR(NN,2,1)

FCUR2=(RKVBA/EIB(IFIX(ABS(REAL(IDELE(
NN)
1)))))*(FCUR(NN,1,2)+FCUR(NN,2,2)+FCUR(NN,3,2))
FCUR1=FCUR1*FIPU
FCUR2=FCUR2*FIPU
IRI=(IFIX(REAL(IDELE(NN))))
IRJ=(IFIX(AIMAG(IDELE(NN))))
CUR1=CABS(FCUR1)
CUR2=CABS(FCUR2)
IF(CUR1.LT.0.001) GO TO 400
WRITE(41,350)IFLT,NN,CUR1,CUR2
350    FORMAT(2I,2F)
400    CONTINUE
500    CONTINUE
DO 600 I=1,IBB
READ(42,525)IL,JL,ALCUR
IF(IL.EQ.0)GO TO 610
IF(REAL(ALCUR).LE.0.0)GO TO 600
BLCUR=CABS(ALCUR)
CLCUR=FIPU*BLCUR*RKVBA/EIB(JL)
BLCUR=FIPU*BLCUR*RKVBA/EIB(IL)
WRITE(43,525)IL,JL,BLCUR,CLCUR
525    FORMAT(2I,2F)

```

```
600      CONTINUE
610      WRITE(41,602)
        WRITE(43,602)
602      FORMAT(' 0 0 0 0 0 0 ')
        CLOSE(UNIT=36)
        CLOSE(UNIT=37)
        CLOSE(UNIT=38)
        CLOSE(UNIT=39)
        CLOSE(UNIT=42)
        CLOSE(UNIT=43)
        STOP
        END
```

\*\*\*\*\*

C TITLE:COORD.F4;USES DATA FROM INPUT.F4,FALT.F4 TO  
COORDINATE

C THE PROTECTION DEVICES FOR THE WHOLE DISTRIBUTION  
SYSTEM.

\*\*\*\*\*

```

OPEN(UNIT=30,FILE='RELA.DAT')
OPEN(UNIT=31,FILE='LOCUR.DAT')
OPEN(UNIT=32,FILE='LCUR.DAT')
OPEN(UNIT=33,FILE='FCUR.DAT')
OPEN(UNIT=34,FILE='TEST.DAT')
OPEN(UNIT=35,FILE='XFOR.DAT')
OPEN(UNIT=36,FILE='DEV.DAT')
OPEN(UNIT=37,FILE='ADEV.DAT')
DIMENSION EB(30),CUREL(200),CURLO(30),Z(100)
1,AIDEVL(30,4),AIDEV(100,7),XFR(200,2),IID(3),RID(100

```

)

```

2,DEV(20,0/4)

```

```

COMPLEX Z,AIDEV,C1,C2,Z1,Z2,RID,CUREL,CU1,CURLO,XFR

```

\*\*\*\*\*

C READ IN LOAD AND BUS VOLTAGE DATA

\*\*\*\*\*

```

READ(30,5)R
5 FORMAT(F)
READ(34,10)IB,E1
10 FORMAT(I,F)
11 READ(30,12)I
12 FORMAT(I)
IF(I.NE.0)GO TO 11
13 READ(30,14)I,E1
14 FORMAT(I,F)
IF(I.EQ.0)GO TO 15
EB(I)=E1
GO TO 13
15 DO 20 I=1,IB
READ(31,16)J,CU2
16 FORMAT(I,F)
IF(J.EQ.0)GO TO 21
CURLO(J)=CMPLX(CU2*1.25,0.0)
20 CONTINUE
21 DO 24 I=1,20
READ(36,22)K,(DEV(I,J),J=0,4)
IF(K.EQ.0)GO TO 23
22 FORMAT(I,5F)
24 CONTINUE

```

\*\*\*\*\*

C NOW TO SET ALL LOAD DEVICES

\*\*\*\*\*

23 TYPE 25

```

25      FORMAT(' ALL LOAD CURRENTS ARE READY,USE DEVICE
NUMBER LIST,')
      DO 100 I=1,IB
      IF(CABS(CURLO(I)).EQ.0)GO TO 100
      ID=I
30      TYPE 35,ID
35      FORMAT(' SELECT THE DEVICE FOR THE LOAD AT
BUS',I3,'...', '$)
      ACCEPT 40,IDEV
      AIDEVL(ID,1)=FLOAT(IDEV)
40      FORMAT(I)
      CURLI=REAL(CURLO(I))
      CALL
      SELECT(CURLI,EB(I),AIDEVL(I,1),AIDEVL(I,2),AIDEVL(I,3)
      1,AIDEVL(I,4))
100      CONTINUE
*****
C      NOW TO BEGIN COORDINATING ELEMENTS IN THE
DISTRIBUTION
*****
110      READ(34,120)NN,I,J,K,R,X
120      FORMAT(4I,2F)
      IF(NN.EQ.0)GO TO 130
      NE=NN
      CI=I
      CJ=J
      RID(NN)=CMPLX(CI,CJ)
      Z(NN)=CMPLX(R,X)
      GO TO 110
130      DO 140 IE=1,NE
      READ(32,135)I,J,CU1
135      FORMAT(2I,2F)
      IF(I.EQ.0)GO TO 140
      IA=0
      CALL SERCH(NE,RID,IE,I,J,IA,IID)
      Z1=0.0*Z1
      Z2=0.0*Z2
      DO 136 IEL=1,IA
      Z1=1/(Z2+Z(IID(IEL)))
      Z2=1/Z1
136      CONTINUE
      DO 138 IEL=1,IA
      CUREL(IID(IA))=(Z2)*(1/Z(IID(IEL)))*CU1
138      CONTINUE
      IF(IA.GT.1)TYPE 101,J
101      FORMAT(' CAUTION THERE IS MORE THAN ONE
SOURCE
140      10F POWER TO THE BUS'14)
      CONTINUE

```

```

DO 150 I=1,NE
  READ(35,145)IJ,J,TINKSH,TWST1,TWST2,TS1
145  FORMAT(2I,4F)
      IF(IJ.EQ.0)GO TO 151
      CALL SERCH(NE,RID,I,IJ,J,IA,IID)
      IA=1
147      XFR(IID(IA),1)=CMPLX(TS1,TINRSH)
          XFR(IID(IA),2)=CMPLX(TWST1,TWST2)
      IA=0
150  CONTINUE
*****
C      NOW TO DETERMINE WHAT ELEMENTS HAVE LOAD BUSES
CONNECTED
*****
151  DO 190 I=1,NE
      IR=IFIX(REAL(RID(I)))
      IM=IFIX(AIMAG(RID(I)))
      IF(AIDVL(IR,1).NE.0) GO TO 155
      IF(AIDVL(IM,1).NE.0)GO TO 156
      GO TO 190
155  II=IFIX(REAL(RID(I)))
      JJ=IFIX(AIMAG(RID(I)))
      GO TO 157
156  II=IFIX(AIMAG(RID(I)))
      JJ=IFIX(REAL(RID(I)))
157  CII=II
      CJJ=JJ
      AIDVL(I,1)=CMPLX(CJJ,CII)
      AIDVL(I,2)=CMPLX(0.0,AIDVL(II,1))
      AIDVL(I,4)=CMPLX(AIDVL(II,2),AIDVL(II,3))
      IF(AIDVL(II,1).GE.35)AIDVL(I,5)=CMPLX(0.0,
1AIDVL(II,4))
      IF(AIDVL(II,1).LT.0)AIDVL(I,7)=CMPLX(0.0,AIDVL(II,4
))
159      TYPE 158,JJ,II
158      FORMAT(' SELECT DEVICE FOR
BUS',I3,' PROTECTING ELEMENT
1FEEDING'/'/' LOAD AT BUS',I4,'...',$)
      ACCEPT 160,IDEV
160  FORMAT(I)
      AIDVL1=FLOAT(IDEV)
      DURR=AIMAG(AIDVL(I,4))
      CURR=REAL(AIDVL(I,4))
      IF(AIMAG(AIDVL(I,2)).GT.0)CURR=10**((DURR)
      CURR=REAL(CUREL(I))
      CALL SELECT(CURR,EB(JJ),AIDVL1,AIDVL2,AIDVL3,CT1)
      CALL
SETDEV(CUREL,I,JJ,II,AIDVL1,AIDVL2,AIDVL3,
1AIDVL,XFR(I,1),XFR(I,2),RE,EB(JJ),EB(II),RID,CT1,DEV

```

```

)
      CT1=0.0
      IF(RE.NE.0)GO TO 159
190    CONTINUE
      IEL=0
200    NEL=NE-IEL
      IF(REAL(AIDDEV(NEL,1)).NE.0)GO TO 300
      INDEX=1
      I=IFIX(REAL(RID(NEL)))
      J=IFIX(AIMAG(RID(NEL)))
      IF(AIMAG(AIDDEV(NEL,2)).NE.0)GO TO 250
205    TYPE 210,J,NEL
      RE=0
210    FORMAT(' ENTER THE DEVICE   FOR THE BUS',I3,' OF
ELEMENT',I4)
      ACCEPT 230,IDEV
230    FORMAT(I)
      IF(IDEV.EQ.100)GO TO 400
      AIDDEV1=FLOAT(IDEV)
      CURR=AIMAG(CUREL(NEL))
      CALL SELECT(CURR,EB(J),AIDDEV1,AIDDEV2,AIDDEV3,CT1)
      IF(AIDDEV1.GT.34)AIDDEV(NEL,5)=CMPLX(0.0,.414973)
      CALL SETDEV(CUREL,NEL,I,J,AIDDEV1,AIDDEV2,AIDDEV3,
1AIDDEV,XFR(NEL,1),XFR(NEL,2),RE,EB(I),EB(J),RID,CT1,D
EV)
      IF(RE.NE.0)GO TO 205
250    TYPE 210,I,NEL
      ACCEPT 230,IDEV
      AIDDEV1=FLOAT(IDEV)
      RE=0
      CURR=REAL(CUREL(NEL))
      CALL SELECT(CURR,EB(I),AIDDEV1,AIDDEV2,AIDDEV3,CT1)
      IF(AIDDEV1.GT.34)AIDDEV(NEL,5)=AIDDEV(NEL,5)+CMPLX(.4149
73,0.0)
      CALL SETDEV(CUREL,NEL,I,J,AIDDEV1,AIDDEV2,AIDDEV3,
1AIDDEV,XFR(NEL,1),XFR(NEL,2),RE,EB(I),EB(J),RID,CT1,D
EV)
      IF(RE.NE.0)GO TO 250
300    IEL=IEL+1
      IF(IEL.LT.NE) GO TO 200
      IF(INDEX.EQ.0)GO TO 400
      IEL=0
      INDEX=0
      GO TO 200
400    TYPE 410
      PRINT 410
410    FORMAT(' DEVICE LISTING')
      DO 440 I=1,NE
      TYPE 420,I,(AIDDEV(I,J),J=1,7)

```

```

      PRINT 420,I,(AIDEV(I,J),J=1,7)
      WRITE(37,420)I,(AIDEV(I,J),J=1,7)
420    FORMAT(I,14F)
44Q    CONTINUE
      WRITE(37,442)
442    FORMAT(' 0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
0.0
      1 0.0 0.0 0.0')
2000   CLOSE(UNIT=30)
      CLOSE(UNIT=31)
      CLOSE(UNIT=32)
      CLOSE(UNIT=33)
      CLOSE(UNIT=34)
      CLOSE(UNIT=36)
      CLOSE(UNIT=37)
      STOP
      END

```

```

*****
*****
C      SUBROUTINE SERCH;FINDS THE ELEMENT CORRESPONDING TO
TWO
C      BUSSES.

```

```

*****
      SUBROUTINE SERCH(NE,RID,NN,I,J,IA,IID)
      DIMENSION RID(100),IID(3)
      COMPLEX RID,C1,C2
      IA=0
      DO 30   IEL=1,100
              CJ=J
              CI=I
              C1=CMPLX(CI,CJ)
              C2=CMPLX(CJ,CI)
              IF(RID(IEI).EQ.C1)GO TO 20
              IF(RID(IEI).EQ.C2)GO TO 20
              GO TO 30
20      IA=IA+1
      IID(IA)=IEL
30      CONTINUE
31      RETURN
      END

```

```

*****
*****
C      SUBROUTINE REFALT;READS FCUR.DAT TO OUTPUT FAULT
CURRENTS
C      AT THE BUSSES
*****
      SUBROUTINE REFALT(IFALT,NEL,FALT,CUREL)
10      READ(33,15)IEF,NN,TFAL,SFAL
15      FORMAT(2I,2F)

```

```

      IF(IEF.EQ.0)GO TO 20
      IF(IEF.NE.IFALT)GO TO 10
      IF(NN.NE.NEL)GO TO 10
      FALT1=TFAL
      FALT2=SFAL
      FALT=AMIN1(FALT1,FALT2)
      FLOCUR=3.0*CUREL
      IF(FALT.LE.FLOCUR)FALT=AMAX1(FALT1,FALT2)
      FALT=AMAX1(FALT1,FALT2)
20    REWIND 33
      RETURN
      END
*****
C      SUBROUTINE SETDEV; SETS THE DEVICE INSTANTANEOUS
ELEMENT
C      DEPENDING ON THE FAULT CURRENT AT THAT BUS
DOES
C      COORDINATE WITH OTHER DEVICES
*****
      SUBROUTINE
      SETDEV(CUREL, IEL, I, J, AIDEV1, AIDEV2, AIDEV3, AIDEV
        1, XFR1, XFR2, RE, EB1, EB2, RID, CT, DEV)
      DIMENSION
      AIDEV(100,7), CUREL(100), DEV(20,0/4), RID(100)
      COMPLEX AIDEV, XFR1, XFR2, CUREL, RID
      IDEV1=IFIX(AIDEV1)
30    IF(IDEV1.LT.0)CALL
      SETREL(CUREL, IEL, I, J, AIDEV, AIDEV1,
        1AIDEV2, AIDEV3, XFR1, XFR2, RE, EB1, EB2, RID, CT, DEV)
      IF(IDEV1.LT.0)GO TO 100
      IF(IDEV1.EQ.99)GO TO 100
      IF(IDEV1.LT.35.AND.IDEV1.GT.0)CALL SETFUS(CUREL(IEL
        1), I, J, IEL, AIDEV, IDEV1, AIDEV2, AIDEV3, XFR1, XFR2, RE, EB1
, EB2,
        2DEV, RID)
      IF(IDEV1.GE.35.AND.IDEV1.LT.99)CALL
      SETCKB(CUREL(IEL),
        1I, J, IEL, AIDEV, IDEV1, AIDEV2, AIDEV3, CT, EB1, EB2)
100    RETURN
      END
*****
*****
C      SUBROUTINE SETFUS; COORDINATES AND SELECTS A FUSE
*****
      SUBROUTINE
      SETFUS(CUREL, I, J, IEL, AIDEV, IDEV1, AIDEV2, AIDEV3
        1, XFR1, XFR2, RE, EB1, EB2, DEV, RID)
      DIMENSION
      AIDEV(100,6), CUREL(100), DEV(20,0/4), RID(100)

```



```

COMPLEX AIDEV,XFR1,XFR2,CUREL,RID
JJ=IFIX(AIMAG(AIDEV(IEL,2)))
IF(JJ.EQ.0)CALL XFDEV(1,J,IEL,AIDEV,COOF)
IF(JJ.NE.0)CALL XFDEV(2,J,IEL,AIDEV,COOF)
IF(JJ.EQ.0)CURR=AIMAG(CUREL(IEL))
IF(JJ.NE.0)CURR=REAL(CUREL(IEL))
IF(JJ.EQ.0.AND.COOF.LT.CURR)COOF=CURR
IF(JJ.NE.0)COOF=(EB2/EB1)*COOF
IF(JJ.NE.0.AND.COOF.LT.CURR)COOF=CURR
IF(IDEV1.LE.15) CALL SFUSE(COOF,IDEV1,OFSET,OFSET1)
IF(IDEV1.GT.15) CALL SBORFU(COOF,IDEV1,OFSET,OFSET1)
IF(JJ.EQ.0) GO TO 20
CI=I
CJ=J
AIDEV(IEL,1)=CMPLX(CI,CJ)
AIDEV(IEL,2)=AIDEV(IEL,2)+CMPLX(FLOAT(IDEV1),0.0)
AIDEV(IEL,3)=CMPLX(OFSET,OFSET1)
GO TO 25
20  CI=I
    CJ=J
    AIDEV(IEL,1)=CMPLX(CI,CJ)
    AIDEV(IEL,2)=CMPLX(0.0,FLOAT(IDEV1))
    AIDEV(IEL,4)=CMPLX(OFSET,OFSET1)
    GO TO 50
25  IF(CABS(XFR1).EQ.0)GO TO 50
    AX=ALOG10((AIMAG(XFR1))/3.0)
    IF(REAL(AIDEV(IEL,2)).LE.15)GO TO 35
    IF(OFSET.LE.AX)CUR=10**AX
    IF(OFSET.LE.AX)CALL SBORFU(CUR,IDEV,OFSET,OFSET1)
    GO TO 40
35  IF(OFSET.LE.AX)CUR=10**AX
    IF(OFSET.LE.AX)CALL SFUSE(CUR,IDEV,OFSET,OFSET1)
40  AIDEV(IEL,2)=CMPLX(FLOAT(IDEV),AIMAG(AIDEV(IEL,2)))
    AIDEV(IEL,3)=CMPLX(OFSET,OFSET1)
    AR=ALOG10(REAL(XFR2))
    CALL FUSE(2,REAL(AIDEV(IEL,2)),AR,OFSET1,TVAL1)
    TVAL=10**TVAL1
    IF(TVAL.GT.2.0)GO TO 43
    GO TO 50
43  TYPE 45
45  FORMAT(' UNABLE TO PUT FUSE IN THIS LOCATION
SUBSTITUE
      1ANOTHER DEVICE')
    RE=1.0
    GO TO 300
50  CALL REFALT(J,IEL,FALT,CUREL(IEL))
    PAUSE 55
    IF(JJ.EQ.0)CALL
SFALT1(AIDEV,CUREL,RID,IEL,I,J,TVAL1,DEV,

```

```

1CVAL)
IF(JJ.NE.0)CALL SFALT2(ADEV, IEL, I, J, TVAL1, DEV,
1FALT, CVAL)
PAUSE 60
ADEV=FLOAT(IDEV1)
55 CALL FUSE(1,ADEV,CVAL,OFFSET,TVAL)
IF(TVAL.GT.TVAL1)GO TO 200
ADEV=ADEV+1
NEGDEV=-IFIX(ADEV)
IF(ADEV.LE.15)CALL SFUSE(COOF,NEGDEV,OFFSET,OFFSET1)
IF(ADEV.GT.15)CALL SBORFU(COOF,NEGDEV,OFFSET,OFFSET1)
GO TO 55
200 IF(JJ.NE.0)GO TO 250
AIDEV(IEL,2)=CMPLX(0.0,ADEV)
AIDEV(IEL,4)=CMPLX(OFFSET,OFFSET1)
GO TO 300
250 AIDEV(IEL,2)=CMPLX(ADEV,AIMAG(AIDEV(IEL,2)))
AIDEV(IEL,3)=CMPLX(OFFSET,OFFSET1)
300 RETURN
END
*****
*****
C SUBROUTINE FUSE; COMPUTES TIME VALUE FOR A GIVEN LOAD
CURRENT
*****
SUBROUTINE FUSE(ID,ADEV,CVAL,OFFSET,TVAL)
TVAL=0.0
IDEV=IFIX(ADEV)
IF(IDEV.GT.15)GO TO 50
X=CVAL-OFFSET
IF(ID.NE.1)GO TO 40
TVAL=4.0480+(-36.4234*X)+(223.7526*(X**2))+(-751.279*
(X**3))
1+(1347.01*(X**4))+(-1222.67*(X**5))+(440.813*(X**6))
TVAL=TVAL-2.0
GO TO 100
40 X=CVAL-OFFSET+.1
TVAL=6.426+(-37.922*X)+(121.909*(X**2))+(-213.420*(X*
*3))+
1(201.771*(X**4))+(-96.9836*(X**5))+(13.6046*(X**6))
TVAL=TVAL-2.0
IF(X.GT.1.4)TVAL=-1.95
GO TO 100
50 X=CVAL-OFFSET
IF(ID.NE.1)GO TO 70
TVAL=3.87693+(-4.262768*X)+(1.219340*(X**2))
TVAL=TVAL-2.0
GO TO 100
70 X=CVAL-OFFSET+.1

```

```

      TVAL=4.614840+(-6.183224*X)+(3.23181*(X**2))+(-.60571
36*(X**3))
      TVAL=TVAL-2.0
100    RETURN
      END
*****
*****
C      SUBROUTINE RELAY; COMPUTES TIME VALUE FOR A GIVEN
CURRENT
C      VALUE FOR A SPECIFIC RELAY
*****
      SUBROUTINE RELAY(NDEV, CURR, TVAL, TDSET, DEV, AMST)
      DIMENSION DEV(20,0/4)
      TVAL=0.0
      X=ALOG10(CURR)
      IF(X.GT.1.2)X=1.2
      DO 10 I=0,4
      TVAL=TVAL+DEV(NDEV,I)*(X**I)
10    CONTINUE
      IF(NDEV.EQ.7)TVAL=TVAL-2.0
      TVAL=TVAL+TDSET
      IF(CURR.GT.AMST.AND.AMST.NE.0)TVAL=-2.0
      RETURN
      END
*****
C      SUBROUTINE CKTBKR; COMPUTES TIME VALUE FOR A GIVEN
CURRENT
C      VALUE
*****
      SUBROUTINE CKTBKR(ID, MDEV, DVAL, OFFSET, TVAL, AMVAL)
      CVAL=DVAL-OFFSET
      IF(ID.NE.1)GO TO 50
      CVAL=CVAL+.1122
      IF(AMVAL.EQ.0.0)AMVAL=10
      IF(CVAL.GT.AMVAL)GO TO 90
      TVAL=5.76908+(-10.88261*(CVAL))+(23.65419*(CVAL**2))+
(-34.7922
      1*(CVAL**3))+(33.77472*(CVAL**4))+(-21.14536*(CVAL**5
))+(6.4
      231778*(CVAL**6))
      TVAL=TVAL-2.0
      GO TO 100
50    CVAL=CVAL+.2315
      AMVAL=AMVAL+.075
      IF(CVAL.GT.AMVAL)GO TO 95
      TVAL=5.8596722+(-4.394335*CVAL)+(-.50690284*(CVAL**2)
)+(10.40
      12739*(CVAL**3))+(-17.064956*(CVAL**4))+(13.011543*(C
VAL**5))

```

```

      2+(-4.010724*(CVAL**6))
      TVAL=TVAL-2.0
      GO TO 100
90      TVAL=-2.0
      GO TO 100
95      TVAL=ALOG10(.025)
100     RETURN
      END
*****
*****
C      SUBROUTINE SETREL;COORDINATES AND SELECTS A RELAY
*****
      SUBROUTINE
SETREL(CUREL, IEL, I, J, AIDEV, AIDEV1, AIDEV2, AIDEV3,
      IXFR1, XFR2, RE, EB1, EB2, RID, CT, DEV)
      DIMENSION
AIDEV(100,7), IIDD(30), RID(100), IID(3), CUREL(100)
      1, DEV(20,0/4), FT(30,2)
      COMPLEX AIDEV, CUREL, XFR1, XFR2, RID
      COOF=0.0
      CURR=0.0
      CDUR=0.0
      TYPE 5
5      FORMAT(' DOES THIS RELAY HAVE AN INST. ELEMENT, IF
YES 0')
      ACCEPT 7, IL
7      FORMAT(I)
      JJ=IFIX(AIMAG(AIDEV(IEL,2)))
      MDEV=IFIX(-AIDEV1)
      IF(JJ.EQ.0)AIDEV(IEL,1)=CMPLX(FLOAT(I),FLOAT(J))
      IF(JJ.EQ.0)AIDEV(IEL,2)=CMPLX(0.0,AIDEV1)
      IF(JJ.NE.0)AIDEV(IEL,2)=CMPLX(AIDEV1,0.0)+AIDEV(IEL,2
)
      IF(JJ.EQ.0)CALL XFDEV(1,J,IEL,AIDEV,COOF)
      IF(JJ.NE.0)CALL XFDEV(2,J,IEL,AIDEV,COOF)
      IF(JJ.EQ.0)CURR=AIMAG(CUREL(IEL))
      IF(JJ.NE.0)CURR=REAL(CUREL(IEL))
      IF(JJ.EQ.0.AND.COOF.LT.CURR)COOF=CURR
      IF(JJ.NE.0)COOF=(EB2/EB1)*COOF
      CDUR=ALOG10(COOF)
      IF(JJ.NE.0.AND.COOF.LT.CURR)COOF=CURR
      IF(CDUR.GT.AIDEV2)AIDEV1=4.0
      IF(CDUR.GT.AIDEV2.AND.JJ.EQ.0)CALL
SELECT(COOF,EB2,AIDEV1,
      1AIDEV2,AIDEV3,CT)
      IF(CDUR.GT.AIDEV2.AND.JJ.NE.0)CALL
SELECT(COOF,EB1,AIDEV1,
      1AIDEV2,AIDEV3,CT)
      CURL=AIMAG(CUREL(IEL))

```

```

IF(JJ.NE.0)AIDEV(IEL,3)=CMPLX(AIDEV2,AIDEV3)
IF(JJ.EQ.0)AIDEV(IEL,4)=CMPLX(AIDEV2,AIDEV3)
IF(JJ.NE.0)CURL=REAL(CUREL(IEL))
IF(JJ.NE.0)AIDEV(IEL,7)=CMPLX(CT,0.0)+AIDEV(IEL,7)
IF(JJ.EQ.0)AIDEV(IEL,7)=CMPLX(0.0,CT)
IF(IL.NE.0)GO TO 100
CALL REFALT(J,IEL,FALT1,CURL)
IF(JJ.NE.0)GO TO 32
FALT1=FALT1*(EB1/EB2)
FALT1=FALT1/(10**(REAL(AIDEV(IEL,4))))
IN=0
DO 10 JI=1,30
    CALL SERCH(1,RID,IEL,J,JI,IA,IID)
    IF(IA.EQ.0)GO TO 10
    DO 8 JA=1,IA
        IN=IN+1
        IIDD(IN)=IID(IA)
8          CONTINUE
10         CONTINUE
DO 30 INN=1,IN
    ID=IIDD(INN)
    IF(ID.EQ.IEL) GO TO 30
    IJ=IFIX(AIMAG(RID(ID)))
    CURJ=AIMAG(CUREL(ID))
    CALL REFALT(IJ,ID,FALT,CURJ)
    FALT2=ALOG10(FALT)
    AID=REAL(AIDEV(ID,2))
    IAID=IFIX(AID)
    IF(IAID.GT.0)GO TO 16
    IF(IAID.LT.0)FALTO=FALT/(10**(REAL(AIDEV(ID,3
))))

    NDEV=-IFIX(REAL(AIDEV(ID,2)))
    KFAL=IFIX(10*FALTO)
    DO 15 K=15,KFAL,10
        RK=K*.1
        IF(ALOG10(RK).GT.1.2)GO TO 16
        CALL
RELAY(NDEV,RK,TVAL1,REAL(AIDEV(ID,6))
    1,DEV,REAL(AIDEV(ID,5)))
        CALL
RELAY(MDEV,RK,TVAL2,TMSET,DEV,0.0)
        TIMEO=(10**TVAL1)+.4
        TIMER=TVAL2
        TIMES=ALOG10(TIMEO)
        TMSET1=TIMES-TIMER
        IF(TMSET1.LE.0)GO TO 15
        TMSET=TMSET1+TMSET
15         CONTINUE
16         IF(IAID.LT.0)GO TO 25

```

```

      OFFSET=AIMAG(AIDDEV(ID,3))
      FNSET=FALT2-OFFSET
      IF(FNSET.GT.1.5)FALT2=OFFSET+1.5
      KVAL=IFIX(10*OFFSET)
      KFAL=IFIX(10*FALT2)
      DO 20 K=KVAL,KFAL
          RK=K*.1
      IF(AID.LT.35)    CALL FUSE(2,AID,RK,OFFSET,TVAL1)
      IF(AID.GE.35)CALL
CKTBKR(2,IFIX(AID),RK,OFFSET,TVAL1,REAL(
      1AIDDEV(IEL,5)))
          CUR=(10**RK)/(10**(REAL(AIDDEV(IEL,3))
      ))
          CALL
RELAY(MDEV,CUR,TVAL2,TMSET,DEV,0.0)
          TIME0=10**TVAL1+.4
          TIMER=TVAL2
          TIMES=ALOG10(TIME0)
          TMSET1=TIMES-TIMER
          IF(TMSET1.LE.0)GO TO 20
          TMSET=TMSET+TMSET1
20          CONTINUE
25          GO TO 30
30          CONTINUE
      AIDDEV(IEL,6)=CMPLX(0.0,TMSET)
      TMSET=0.0
      GO TO 45
32      AID=AIMAG(AIDDEV(IEL,2))
      FALT2=ALOG10(FALT1)
      IF(AID.GT.0)GO TO 35
      FALT1=FALT1*(EB1/EB2)
      IF(AID.LT.0)FALT=FALT1/(10**(REAL(AIDDEV(IEL,4))))
      NDEV=-IFIX(AIMAG(AIDDEV(IEL,2)))
      KFAL=IFIX(FALT*10)
      DIF=KFAL-15
      ID=IFIX(DIF/50)
      IF(ID.LE.0)ID=1
      DO 33 K=15,KFAL,ID
          RK=K*.1
      RK2=RK*(EB2/EB1)*(10**(REAL(AIDDEV(IEL,4)))/10**
      1(REAL(AIDDEV(IEL,3))))
          IF(RK.GT.20)GO TO 34
          CALL
RELAY(NDEV,RK,TVAL1,AIMAG(AIDDEV(IEL,6)),DEV,
      1AIMAG(AIDDEV(IEL,5)))
          CALL RELAY(MDEV,RK2,TVAL2,TMSET,DEV,0.0)
          TIME0=10**TVAL1+.4
          TIMES=ALOG10(TIME0)
          TIMER=TVAL2

```

```

          TMSET1=TIMES-TIMER
          IF(TMSET1.LE.0)GO TO 33
          TMSET=TMSET1+TMSET
33      CONTINUE
34      AIDEV(IEL,6)=AIDEV(IEL,6)+CMPLX(TMSET,0.0)
35      TMSET=0.0
          IF(AID.LT.0)GO TO 45
          OFFSET=AIMAG(AIDEV(IEL,4))
          FNSET=FALT2-OFFSET
          IF(FNSET.GT.1.5)FALT2=OFFSET+1.5
          KVAL=IFIX(10*OFFSET)
          KFAL=IFIX(10*FALT2)
          DO 40 K=KVAL,KFAL
              RK=K*.1
              IF(AID.LT.35)CALL FUSE(2,AID,RK,OFFSET,TVAL1)
              IF(AID.GE.35)CALL
CKTBKR(2,IFIX(AID),RK,OFFSET,TVAL1,AIMAG(
1AIDEV(IEL,5)))
                  CUR=RK-REAL(AIDEV(IEL,3))
                  CURTA=10**CUR
                  CUR=(EB2/EB1)*(10**RK)
                  CURTA=CUR/(10**(REAL(AIDEV(IEL,3))))
                  IF(CURTA.LT.1.5)GO TO 40
                  CALL RELAY(MDEV,CURTA,TVAL2,TMSET,DEV,0.0)
                  TIMEO=10**TVAL1+.4
                  TIMER=TVAL2
                  TIMES=ALOG10(TIMEO)
                  TMSET1=TIMES-TIMER
                  IF(TMSET1.LE.0)GO TO 40
                  TMSET=TMSET+TMSET1
40      CONTINUE
          AIDEV(IEL,6)=AIDEV(IEL,6)+CMPLX(TMSET,0.0)
45      TMSET=0.0
          IF(JJ.EQ.0.AND.FALT1.GT.6)FALT1=6
          IF(IL.EQ.0.AND.JJ.EQ.0)AIDEV(IEL,5)=CMPLX(0.0,FALT1)
          FALT1=FALT1/(10**REAL(AIDEV(IEL,3)))
          IF(FALT1.GT.6)FALT1=6
          IF(IL.EQ.0.AND.JJ.NE.0)AIDEV(IEL,5)=AIDEV(IEL,5)+CMPL
X(FALT1,
10.0)
100     RETURN
        END
*****
C      SUBROUTINE SFALT1;PROVIDES THE DEVICE WITH THE
LONGEST
C      TIME AT FAULT,FIRST DEV IN ELEMENT.
*****
        SUBROUTINE SFALT1(AIDEV,CUREL,RID,IEL,I,J,TVAL,DEV,
1CVAL)

```

```

      DIMENSION AIDEV(100,6),CUREL(100),RID(100),IID(3),
      IIDD(30),DEV(20,0/4)
      COMPLEX AIDEV,CUREL,RID
      DO 10 JI=1,30
        CALL SERCH(1,RID,IEL,J,JI,IA,IID)
        IF(IA.EQ.0)GO TO 10
        DO 8 JA=1,IA
          IN=IN+1
          IIDD(IN)=IID(IA)
8          CONTINUE
10         CONTINUE
      DO 30 INN=1,IN
        ID=IIDD(INN)
        IJ=IFIX(AIMAG(RID(ID)))
        CURJ=AIMAG(CUREL(ID))
        CALL REFALT(IJ,ID,FALT,CURJ)
        FALT2=ALOG10(FALT)
        AID=REAL(AIDEV(ID,2))
        IAID=IFIX(AID)
        IF(IAID.GT.32)GO TO 100
        FALT2=REAL(AIDEV(IEL,4))+.5
        FALTO=10**(FALT2)
        IF(IAID.LT.0)FALT=FALTO/(10**(REAL(AIDEV(ID,3
))))
        NDEV=-IFIX(REAL(AIDEV(ID,2)))
        IF(IAID.LT.0)CALL RELAY(NDEV,FALT,TVAL1,REAL
1(AIDEV(ID,6)),DEV,REAL(AIDEV(ID,5)))
        FAL=REAL(AIDEV(IEL,4))+.5
        IF(FAL.LT.FALT2)FALT2=FAL
        IF(IAID.GT.0)CALL
FUSE(2,AID,FALT2,AIMAG(AIDEV
1(ID,3)),TVAL1)
        IF(TVAL.GE.TVAL1)GO TO 25
        GO TO 30
25        IF(IAID.LT.0)CVAL=-FALT2
        CVAL=FAL
        TVAL=TVAL1

30        CONTINUE
100       RETURN
          END
*****
*****
C        SUBROUTINE SFALT2;AS IN 1,COMPUTES TIME FOR LOAD
SIDE OF
C        ELEMENT AT FALT.
*****
      SUBROUTINE SFALT2(AIDEV,IEL,I,J,TVAL1,DEV,FALT,CVAL)
      DIMENSION AIDEV(100,6),DEV(20,0/4)
      COMPLEX AIDEV

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```

      FALT2=ALOG10(FALT)
      AID=AIMAG(AIDDEV(IEL,2))
      FAL=REAL(AIDDEV(IEL,3))+.5
      FALT=10**(FAL)
      FALT3=FALT/(10**(AIMAG(AIDDEV(IEL,3))))
      IF(AID.LT.0)CALL
RELAY(NDEV,FALT3,TVAL1,AIMAG(AIDDEV(IEL
1,6)),DEV,AIMAG(AIDDEV(IEL,5)))
      IF(FAL.LT.FALT2)FALT2=FAL
      IF(AID.GT.0)CALL FUSE(2,AID,FAL,AIMAG(AIDDEV(IEL,4))
1,TVAL1)
      CVAL=FALT2
      RETURN
      END
*****
*****
      SUBROUTINE XFDEV(NN,I,IEL,AIDDEV,COOF)
      DIMENSION IID(30),AIDDEV(100,6)
      COMPLEX AIDDEV
      COOF=0.0
      IX=0
      IF(NN.NE.1)GO TO 50
      DO 30 IA=1,100
          AID=REAL(AIDDEV(IA,1))
          IF(IFIX(AID).NE.1)GO TO 30
          IX=IX+1
          IID(IX)=IA
30      CONTINUE
      DO 32 K=1,IX
32      CONTINUE
      DO 40 JA=1,IX
          OFFSET=AIMAG(AIDDEV(IID(JA),3))
          IF(REAL(AIDDEV(IID(JA),2)).LT.0)OFFSET=REAL(AID
EV(
          IID(JA),3))
          IF(REAL(AIDDEV(IID(JA),2)).GE.35)OFFSET=REAL(AI
DEV(
          IID(JA),5))+OFFSET-.05
          IF(AIMAG(AIDDEV(IEL,2)).LT.0.AND.REAL(AIDDEV(II
D
          1(JA),2)).GT.0.AND.REAL(AIDDEV(IID(JA),2)).LT.35)
          2OFFSET=OFFSET+.15
          IF(COOF.GT.OFFSET)GO TO 40
          COOF=OFFSET
40      CONTINUE
      GO TO 60
50      IF(AIMAG(AIDDEV(IEL,2)).GT.0)COOF=AIMAG(AIDDEV(IEL,4))
      IF(AIMAG(AIDDEV(IEL,2)).LT.0)COOF=REAL(AIDDEV(IEL,4))
      IF(AIMAG(AIDDEV(IEL,2)).GE.35)COOF=AIMAG(AIDDEV(IEL,5))

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```

-.075      1+COOF
            IF(REAL(AIDDEV(IEL,2)).LT.0.AND.AIMAG(AIDDEV(IEL,2)).GT
.0          1.AND.AIMAG(AIDDEV(IEL,2)).LT.35)COOF=COOF+.15
60          COOF=COOF+.025
            DOOF=10**(COOF)
            COOF=DOOF
            RETURN
            END
*****
*****
C          SUBROUTINE SETCKB;CORDINATES AND SELECTS A THERMAL
MAGNETIC
C          BREAKER.
*****
*****
          SUBROUTINE SETCKB(CUREL,I,JJ,IEL,AIDDEV,IDEV,OFFSET
          1,OFFSET1,AMAG,EB1,EB2)
          DIMENSION AIDDEV(100,7),CON(5)
          COMPLEX AIDDEV,CUREL
          CON(1)=2.6
          CON(2)=3.5
          CON(3)=5.0
          CON(4)=6.0
          CON(5)=7.0
          J=IFIX(AIMAG(AIDDEV(IEL,1)))
          IF(J.EQ.0)CALL XFDEV(1,J,IEL,AIDDEV,COOF)
          IF(J.NE.0)CALL XFDEV(2,J,IEL,AIDDEV,COOF)
          IF(J.EQ.0)DOOF=ALOG10(COOF)-AIMAG(AIDDEV(IEL,5))
          IF(J.EQ.0)COOF=10**DOOF
          IF(J.NE.0)DOOF=ALOG10(COOF)-AIMAG(AIDDEV(IEL,5))
          IF(J.NE.0)COOF=10**DOOF
          IF(J.EQ.0)CURR=AIMAG(CUREL)
          IF(J.NE.0)CURR=REAL(CUREL)
          IF(EB1.NE.EB2)GO TO 45
          IF(COOF.LT.CURR)COOF=CURR
          GO TO 46
45          RE2=(EB2/EB1)*COOF
          IF(RE2.GE.CURR)COOF=RE2
          IF(RE2.LT.CURR)COOF=CURR
46          CALL SBRKR(COOF,IDEV3,OFFSET,OFFSET1,DMNY)
          IF(IDEV.LT.IDEV3)IDEV=IDEV3
          IF(IDEV.GE.IDEV3)IDEV=IDEV+1
          CI=I
          CJ=JJ
          AIDDEV(IEL,1)=CMPLX(CI,CJ)
          IF(J.EQ.0)AIDDEV(IEL,2)=CMPLX(0.0, FLOAT(IDEV))
          IF(J.NE.0)AIDDEV(IEL,2)=CMPLX(FLOAT(IDEV),0.0)+AIDDEV

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```

1( IEL, 2)
IF( J.EQ.0) AIDEV( IEL, 4)=CMPLX( OFSET, OFSET1)
IF( J.NE.0) AIDEV( IEL, 3)=CMPLX( OFSET, OFSET1)
IF( J.EQ.0) FLT=4*AIMAG( CUREL)
IF( J.NE.0) FLT=4*REAL( CUDEL)
SET=10** (OFSET-.12)
DO 50 K=1, 5
      TRP=CON( K)*SET
      IF( TRP.GT. FLT) GO TO 60
50    CONTINUE
60    IF( AMAG.NE.0) AMAG=ALOG10( CON( K))
      IF( J.EQ.0) AIDEV( IEL, 5)=CMPLX( 0.0, AMAG)
      IF( J.NE.0) AIDEV( IEL, 5)=CMPLX( AMAG, 0.0)+AIDEV( IEL, 5)
      RETURN
      END
*****
*****
C      SUBROUTINE SELECT; SELECTS A PARTICULAR DEVICE
*****
      SUBROUTINE SELECT( CURLO, EB, ADEVL1, ADEVL2, ADEVL3, CT)
      IDEVL1=IFIX( ADEVL1)
54    IF( IDEVL1.EQ.0) GO TO 99
      IF( IDEVL1.EQ.1) GO TO 60
      IF( IDEVL1.EQ.2) GO TO 70
      IF( IDEVL1.EQ.4) GO TO 80
      IF( IDEVL1.GT.4) GO TO 53
      GO TO 58
53    TYPE 55
55    FORMAT( ' NO SUCH DEVICE OR DEVICE ERROR, RE-ENTER
1 DEVICE NR 1-4..., ' $)
      ACCEPT 56, IDEVL1
56    FORMAT( I)
      GO TO 54
58    IF( EB.GT.600.0) GO TO 53
      CALL SBRKR( CURLO, IDEVL1, ADEVL2, ADEVL3, ADEVL4)
      ADEVL1=FLOAT( IDEVL1)
      CT=ADEVL4
      GO TO 100
60    CALL SFUSE( CURLO, IDEVL1, ADEVL2, ADEVL3)
      ADEVL1=FLOAT( IDEVL1)
      GO TO 100
70    IF( EB.LT.600) GO TO 53
      CALL SBORFU( CURLO, IDEVL1, ADEVL2, ADEVL3)
      ADEVL1=FLOAT( IDEVL1)
      GO TO 100
80    CALL SRELA( CURLO, IDEVL1, NTAP, NCT, PKUP, CT)
      ADEVL1=IDEVL1
      ADEVL2=PKUP
      ADEVL3=NCT*100+NTAP

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          GO TO 100
99      ADEVL1=99
        ADEVL2=CURLO
        ADEVL3=CURLO
100     CONTINUE
        RETURN
        END
*****
C      SUBROUTINE SFUSE;USED TO SELECT A CURRENT LIMITING
FUSE
C      THIS MAY BE EITHER HIGH OR LOW VOLTAGE
*****
          SUBROUTINE SFUSE(CURLO,NDEV,OFFSET,OFFSET1)
          IF(NDEV.LT.0)GO TO 10
          DEV=-11.15221+(23.865*ALOG10(CURLO))-(16.487*(ALOG10(
CURLO
          1)**2))+(2.9288*(ALOG10(CURLO)**3))+(3.19672*(ALOG10(
CU
          2RLO)**4))-(1.48877*(ALOG10(CURLO)**5))+(.1776431*(AL
OG
          310(CURLO)**6))
          NDEV=IFIX(DEV)+1
          IF(NDEV.GT.15)NDEV=15
10      DEV=ABS(FLOAT(NDEV))
          OFFSET=-.9532-(.046433*DEV)+(.117885*(DEV**2))+(-.02935
2*(DEV
          1**3))+(.00337*(DEV**4))+(-.0001847*(DEV**5))+(.00000
39*(
          2DEV**6))
          OFFSET1=OFFSET+.1
          IF(NDEV.LT.-15)NDEV=-15
          IF(NDEV.GT.15)NDEV=15
          RETURN
          END
*****
C      SUBROUTINE SBORFU;USED TO SELECT A BORIC ACID HIGH
VOLTAGE
C      FUSE
*****
          SUBROUTINE SBORFU(CURLO,NDEV,OFFSET,OFFSET1)
          ALOGC=ALOG10(CURLO)
          IF(NDEV.LT.0)GO TO 10
          DEV=88.1643+(-215.2235*(ALOGC))+(188.225*(ALOGC**2))+
(-69.
          13463*(ALOGC**3))+(7.4695*(ALOGC**4))+(1.65257*(ALOGC
**5))+
          2(-.347786*(ALOGC**6))
          NDEV=IFIX(DEV)+1
          IF(NDEV.GT.19)NDEV=19.

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10      DEV=ABS(FLOAT(NDEV))
        IF(NDEV.LT.0)DEV=DEV-15
        OFFSET=1.366111+.1134579*DEV+(-.0012654*(DEV**2))+(.00
00213*  1(DEV**3))
        OFFSET1=OFFSET+.1
        IF(NDEV.LT.-19)NDEV=-19
        IF(NDEV.GT.19)NDEV=19
        IF(NDEV.LT.0)NDEV=-NDEV+15
        IF(NDEV.GT.0)NDEV=NDEV+15
        RETURN
        END
*****
C      SUBROUTINE SBRKR;USED TO SELECT A THERMAL MAGNETIC
BREAKER
*****
        SUBROUTINE SBRKR(CURLO,NDEV,OFFSET,OFFSET1,AMAG)
        DIMENSION CON(5)
        CON(1)=2.6
        CON(2)=3.5
        CON(3)=4.6
        CON(4)=5.6
        CON(5)=7.0
        TYPE 10
10      FORMAT(' ENTER MANUFACTURER (N.A. AT PRESENT USE
FOR FUTURE
        IEXPANSION)')
        TYPE 25
25      FORMAT(' INPUT TEMPERATURE FOR AMBIENT SHIFT,1 FOR
LESS THAN
        110 DEG C,2 FOR 60 DEG C, '/'<CR>FOR NO SHIFT..')
        ACCEPT 28,IOFF
28      FORMAT(I)
        IF(IOF.EQ.1)OFS=-.1
        IF(IOF.EQ.2)OFS=.05
        IF(MAN.NE.0)GO TO 80
        IF(CURLO.LE.600.)GO TO 30
        IF(CURLO.LE.800.)GO TO 50
        GO TO 70
30      IF(CURLO.LT.300.)MDEV=1
        IF(CURLO.LT.300.)OFFSET=2.47712
        IF(CURLO.GT.300.0.AND.CURLO.LE.350.)MDEV=2
        IF(CURLO.GT.300.0.AND.CURLO.LE.350.)OFFSET=2.54407
        IF(CURLO.GT.350.0.AND.CURLO.LE.400.)MDEV=3
        IF(CURLO.GT.350.0.AND.CURLO.LE.450.)OFFSET=2.60206
        IF(CURLO.GT.400.0.AND.CURLO.LE.450.)MDEV=4
        IF(CURLO.GT.400.0.AND.CURLO.LE.450.)OFFSET=2.65321
        IF(CURLO.GT.450.0.AND.CURLO.LE.500.)MDEV=5
        IF(CURLO.GT.450.0.AND.CURLO.LE.500.)OFFSET=2.69897

```

```

      IF(CURLO.GT.500.)MDEV=6
      IF(CURLO.GT.500.)OFSET=2.77815
      GO TO 80
50    IF(CURLO.LE.700.)MDEV=7
      IF(CURLO.LE.700.)OFSET=2.8451
      IF(CURLO.GT.700.)MDEV=8
      IF(CURLO.GT.700.)OFSET=2.90309
      GO TO 80
70    IF(CURLO.LE.1000.)MDEV=9
      IF(CURLO.LE.1000.)OFSET=3.0
      IF(CURLO.GT.1000.)MDEV=10
      IF(CURLO.GT.1000.)OFSET=3.3
80    NDEV=MDEV+34
      OFSET=OFSET+OFS+.1122
      OFSET1=OFSET+.12
      TYPE 90
90    FORMAT(' DOES THE DEVICE HAVE A MAGNETIC
ELEMENT?(0)YES.')
      ACCEPT 95,NOEL
95    FORMAT(I)
      FCUR=4*CURLO
      SET=10**(OFSET-.12)
      DO 100 I=1,5
          TD=SET*CON(I)
          IF(TD.GT.FCUR)GO TO 105
100   CONTINUE
105   AMAG=ALOG10(CON(I))
      IF(NOEL.NE.0)AMAG=0.0
      RETURN
      END
*****
C      SUBROUTINE SRELA;USED TO SELECT A RELAY
*****
      SUBROUTINE SRELA(CURLO,NDEV,NTAP,NCT,PKUP,CT)
      TYPE 10
10    FORMAT(' SELECT MANUFACTUER (FUTURE EXPANSION)')
      TYPE 20
20    FORMAT(' SELECT THE WESTINGHOUSE CO RELAY ,REFER TO
TABLE',S)
      ACCEPT 25,NUM
25    FORMAT(I)
      NDEV=-NUM
      IF(CURLO.LT.30)CT=10
      IF(CURLO.GE.30.AND.CURLO.LT.120)CT=30
      IF(CURLO.GE.120)CT=120
      IF(CT.EQ.10)NCT=1
      IF(CT.EQ.30)NCT=2
      IF(CT.EQ.120)NCT=3
      TAP=CURLO/CT

```

```
IF(TAP.LE.1.0)GO TO 71
IF(TAP.LE.1.2)GO TO 72
IF(TAP.LE.1.5)GO TO 73
IF(TAP.LE.2.0) GO TO 74
IF(TAP.LE.2.5)GO TO 75
IF(TAP.LE.3.0)GO TO 76
IF(TAP.LE.3.5)GO TO 77
IF(TAP.LE.4.0)GO TO 78
IF(TAP.LE.5.0)GO TO 79
IF(TAP.LE.6.0)GO TO 80
IF(TAP.LE.7.0)GO TO 81
IF(TAP.LE.8.0)GO TO 82
IF(TAP.LE.10.0)GO TO 83
GO TO 84
71 NTAP=1
TAP=1.0
GO TO 90
72 NTAP=2
TAP=1.2
GO TO 90
73 NTAP=3
TAP=1.5
GO TO 90
74 NTAP=4
TAP=2.0
GO TO 90
75 NTAP=5
TAP=2.5
GO TO 90
76 NTAP=6
TAP=3.0
GO TO 90
77 NTAP=7
TAP=3.5
GO TO 90
78 NTAP=8
TAP=4.0
GO TO 90
79 NTAP=9
TAP=5.0
GO TO 90
80 NTAP=10
TAP=6.0
GO TO 90
81 NTAP=11
TAP=7.0
GO TO 90
82 NTAP=12
TAP=8.0
```

```
83      GO TO 90  
        NTAP=13 .  
        TAP=10.0  
        GO TO 90  
84      NTAP=14  
        TAP=12.0  
90      PKUP=ALOG10(TAP*CT)  
        RETURN  
        END
```



```

C      TITLE:PLOTD.F4;PLOTS DEVICES FROM COORD.F4
*****
      OPEN(UNIT=30,FILE='ADEV.DAT')
      OPEN(UNIT=31,FILE='DEV.DAT')
      OPEN(UNIT=32,FILE='RELA.DAT')
      OPEN(UNIT=33,FILE='FCUR.DAT')
      OPEN(UNIT=34,FILE='TEST.DAT')
      EXTERNAL T25HAN
      DIMENSION EB(30),DEV(20,0/4),AIDEV(100,7),RID(100)
      COMPLEX AIDEV,RID
      READ(32,3)R
3      FORMAT(F)
5      READ(32,10)I
10     FORMAT(I)
      IF(I.NE.0)GO TO 5
15     READ(32,20)I,E1
20     FORMAT(I,F)
      IF(I.EQ.0)GO TO 25
      EB(I)=E1
      GO TO 15
25     DO 40 K=1,100
      READ(30,30)I,(AIDEV(I,J),J=1,7)
30     FORMAT(I,14F)
      IF(I.EQ.0)GO TO 45
40     CONTINUE
45     READ(34,50)IB,E1
50     FORMAT(I,F)
55     READ(34,60)NN,I,J,K,R,X
60     FORMAT(4I,2F)
      IF(NN.EQ.0) GO TO 70
      NE=NN
      CI=I
      CJ=J
      RID(NN)=CMPLX(CI,CJ)
      GO TO 55
70     DO 80 I=1,20
          READ(31,75)K,(DEV(I,J),J=0,4)
75     FORMAT(I,5F)
      IF(K.EQ.0)GO TO 400
80     CONTINUE
400    TYPE 410
410    FORMAT(' DEVICE LISTING')
      DO 440 I=1,NE
      TYPE 420,I,(AIDEV(I,J),J=1,7)
      PRINT 420,I,(AIDEV(I,J),J=1,7)
420    FORMAT(I,14F)
440    CONTINUE
445    TYPE 450
450    FORMAT(' DEVICES HAVE BEEN SLT IF YOU WANT TO PLOT

```

```

GRAPH PAPER
      1 ENTER(0),IF NOT TYPE(1)')
      ACCEPT 456,IP
456    FORMAT(I)
      IF(IP.NE.0)GO TO 480
      TYPE 460
460    FORMAT(' THIS WILL PLOT CURVES BASED TO THE LOWEST
VOLTAGE
      1 IN THE SYSTEM.')
      TYPE 461
461    FORMAT(' INPUT THE CURRENT OFFSET FOR THE
GRAPH,INTEGER..')
      ACCEPT 462,IAOFF
462    FORMAT(I)
      CALL INITT
      CALL LOG(IAOFF)
      CALL FLUSH
480    TYPE 485
485    FORMAT(' INPUT ELEMENT ..')
      ACCEPT 490,IEL
490    FORMAT(I)
      I=IFIX(REAL(RID(IEL)))
      J=IFIX(AIMAG(RID(IEL)))
      EB1=EB(1)
      DO 495 K=1,IB
          EB1=AMIN1(EB1,EB(K))
495    CONTINUE
550    FAC=ALOG10(EB(I)/EB1)-IAOFF
      FAC1=ALOG10(EB(J)/EB1)-IAOFF
      CUR=REAL(AIDDEV(IEL,3))
      CUR1=REAL(AIDDEV(IEL,4))
      CUR2=AIMAG(AIDDEV(IEL,3))
      CUR3=AIMAG(AIDDEV(IEL,4))
*****
C      NOW TO PLOT LOAD SIDE OF THE ELEMENT
*****
      CALL REFALT(J,IEL,FALT,900.0)
      IF(AIMAG(AIDDEV(IEL,2)).GT.0) GO TO 585
      STL=REAL(AIDDEV(IEL,4))
      STP=FALT/10**STL
      IF(AIMAG(AIDDEV(IEL,5)).NE.0)STP=AIMAG(AIDDEV(IEL,5))
      ST1=ALOG10(FALT)
      YM=(STL+FAC1)*190+175.0
      XM=0.0
      CALL MOVEA(XM,YM)
      STP=10*STP
      ITP=IFIX(STP)
      IF(ITP.LT.15)TYPE 575
575    FORMAT(' THE LOAD SIDE RELAY WILL NOT BE VERY

```

## SENSITIVE

```

      1 TO A FAULT')
      IDEV=IFIX(ABS(AIMAG(AIDDEV(IEL,2))))
      TYPE 570, IDEV, ITP
570   FORMAT(' IDEV,', 2I)
      DIF=ITP-15.
      ID=IFIX(DIF/200.0)
      IF(ID.LE.0) ID=1
      TVAL3=10.0
      TDSET=AIMAG(AIDDEV(IEL,6))
      DO 580 K=15, ITP, ID
          RK=.1*(FLOAT(K))
          CALL RELAY(IDEV, RK, TVAL, TDSET, DEV)
          IF(TVAL.GT.TVAL3) TVAL=TVAL3
          TVAL3=TVAL
          T=900-((TVAL+2.0)*180)
          R=(ALOG10(RK)+FAC1+STL)*190+175.0
          CALL DRAWA(T, R)
580   CONTINUE
      PAUSE 4
      IF(AIMAG(AIDDEV(IEL,5)).NE.0) CALL DRAWA((900.0), R)
      GO TO 591
585   OFFSET=CUR1
      M=IFIX(80*OFFSET)
      ADEV=AIMAG(AIDDEV(IEL,2))
      KIM=IFIX(100*(ALOG10(FALT)))
      DO 587 K=M, KIM
          CVAL=K*.01
          IF(ADEV.LT.35) CALL FUSE(1, ADEV, CVAL, OFFSET, TVAL)
          IF(ADEV.GE.35) CALL
CKTBKR(1, IFIX(ADEV), CVAL, OFFSET, TVAL,
      1 AIMAG(AIDDEV(IEL,5)))
          TVAL=TVAL+2.0
          IF(TVAL2.LT.TVAL.AND.ND.NE.0) GO TO 539
          TVAL2=TVAL
          ND=1
          CALL
DRAWA(900-((TVAL)*180), (CVAL+FAC1)*190+175.0)
537   CONTINUE
589   OFFSET=CUR3
      CALL MOVEA(0.0, 0.0)
      ND=0
      M=IFIX(80*OFFSET)
      DO 588 K=M, KIM
          CVAL=K*.01
          IF(ADEV.LT.35) CALL FUSE(2, ADEV, CVAL, OFFSET, TVAL)
          IF(ADEV.GE.35) CALL
CKTBKR(2, IFIX(ADEV), CVAL, OFFSET, TVAL,
      1 AIMAG(AIDDEV(IEL,5)))

```

```

        TVAL=TVAL+2.0
        IF(TVAL2.LT.TVAL.AND.ND.NE.0)GO TO 591
        TVAL2=TVAL
        ND=1
        CALL
DRAWA(900-((TVAL)*180),(CVAL+FAC1)*190+175.0)
588      CONTINUE
*****
C        NOW TO DRAW THE LINE SIDE
*****
591      CALL MOVEA(0.0,0.0)
        AID=(REAL(AIDDEV(IEL,2)))
        IF(AID.GT.0)GO TO 595
        IDEV=IFIX(-AID)
        STL=REAL(AIDDEV(IEL,3))
        STP=FALT/10**STL
        IF(REAL(AIDDEV(IEL,5)).NE.0)STP=REAL(AIDDEV(IEL,5))
        YM=(STL+FAC)*190+175.0
        XM=0.0
        CALL MOVEA(XM,YM)
        STP=STP*10
        ITP=IFIX(STP)
        DIF=ITP-15
        ID=IFIX(DIF/200.0)
        IF(ID.LE.0)ID=1
        TVAL3=10.0
        TDSET=REAL(AIDDEV(IEL,6))
        DO 590 K=15,ITP,ID
            RK=K*.1
            CALL RELAY(IDEV,RK,TVAL,TDSET,DEV)
            IF(TVAL.GT.TVAL3)TVAL=TVAL3
            TVAL3=TVAL
            CALL
DRAWA(900-((TVAL+2.0)*180),((ALOG10(RK)+STL
        1+FAC)*190+175.0))
590      CONTINUE
        IF(REAL(AIDDEV(IEL,5)).NE.0)CALL
DRAWA((900.0),((ALOG10(RK)+
        1STL+FAC)*190+175.0))
595      IF(REAL(AIDDEV(IEL,2)).LT.0)GO TO 598
        OFFSET=CUR
        ADEV=REAL(AIDDEV(IEL,2))
        ND=0
        M=IFIX(80*OFFSET)
        KIM=IFIX(100*ALOG10(FALT))
        DO 597 K=M,KIM
            CVAL=K*.01
            IF(ADEV.LE.34)CALL FUSE(1,ADEV,CVAL,OFFSET,TVAL)
            IF(ADEV.GE.35)CALL

```

```

CKTBKR(1,IFIX(ADEV),CVAL,OFFSET,TVAL,
      1REAL(AIDV(1EL,5)))
      TVAL=TVAL+2.0
      IF(TVAL2.LT.TVAL.AND.ND.NE.0)GO TO 601
      TVAL2=TVAL
      ND=1
      CALL
DRAWA(900-(TVAL*180),(CVAL+FAC)*190+175.0)
597      CONTINUE
601      OFFSET=CUR2
      CALL MOVEA(0.0,0.0)
      ND=0
      M=IFIX(80*OFFSET)
      DO 599 K=M,KIM
          CVAL=K*.01
      IF(ADEV.LE.34)CALL FUSE(2,ADEV,CVAL,OFFSET,TVAL)
      IF(ADEV.GE.35)CALL
CKTBKR(2,IFIX(ADEV),CVAL,OFFSET,TVAL,
      1REAL(AIDV(1EL,5)))
      TVAL=TVAL+2.0
      IF(TVAL2.LT.TVAL.AND.ND.NE.0)GO TO 598
      TVAL2=TVAL
      ND=1
      CALL
DRAWA(900-(TVAL*180),(CVAL+FAC)*190+175.0)
599      CONTINUE
598      TYPE 600
600      FORMAT(' FINISHED??')
      ND=0
      CALL MOVEA(0.0,0.0)
      CALL FLUSH
      ACCEPT 610,I
610      FORMAT(I)
      IF(I.EQ.0)GO TO 2000
      GO TO 445
2000      CLOSE(UNIT=30)
      CLOSE(UNIT=31)
      CLOSE(UNIT=32)
      CLOSE(UNIT=33)
      CLOSE(UNIT=34)
      CALL FINITT(0,0)
      STOP
      END
*****
C      SUBROUTINE REFALT;READS FCUR.DAT TO OUTPUT FAULT
CURRENTS
C      AT THE BUSES
*****
      SUBROUTINE REFALT(1FALT,NEL,FALT,CUREL)

```

```

10      READ(33,15)IEF,NN,TFAL,SFAL
15      FORMAT(2I,2F)
        IF(IEF.EQ.0)GO TO 20
        IF(IEF.NE.IFALT)GO TO 10
        IF(NN.NE.NEL)GO TO 10
        FALT1=TFAL
        FALT2=SFAL
        FALT=AMIN1(FALT1,FALT2)
        FLOCUR=3.0*CUREL
        IF(FALT.LE.FLOCUR)FALT=AMAX1(FALT1,FALT2)
        FALT=AMAX1(FALT1,FALT2)
20      REWIND 33
        RETURN
        END
*****
C      SUBROUTINE FUSE; COMPUTES TIME VALUE FOR A GIVEN LOAD
CURRENT
*****
        SUBROUTINE FUSE(ID,ADEV,CVAL,OFFSET,TVAL)
        TVAL=0.0
        IDEV=IFIX(ADEV)
        IF(IDEV.GT.15)GO TO 50
        X=CVAL-OFFSET
        IF(ID.NE.1)GO TO 40
        TVAL=4.0480+(-36.4234*X)+(223.7526*(X**2))+(-751.279*
(X**3))
        1+(1347.01*(X**4))+(-1222.67*(X**5))+(-440.813*(X**6))
        TVAL=TVAL-2.0
        GO TO 100
40      X=CVAL-OFFSET+.1
        TVAL=6.426+(-37.922*X)+(121.909*(X**2))+(-213.420*(X*
*3))+
        1(201.771*(X**4))+(-96.9836*(X**5))+(-18.6046*(X**6))
        TVAL=TVAL-2.0
        IF(X.GT.1.4)TVAL=-1.95
        GO TO 100
50      X=CVAL-OFFSET
        IF(ID.NE.1)GO TO 70
        TVAL=3.876979+(-4.262768*X)+(1.21940*(X**2))
        TVAL=TVAL-2.0
        GO TO 100
70      X=CVAL-OFFSET+.1
        TVAL=4.614841+(-6.173224*X)+(3.231806*(X**2))+(-.6057
136*(X**3))
        TVAL=TVAL-2.0
100     RETURN
        END
*****
C      SUBROUTINE RELAY; COMPUTES TIME VALUE FOR A GIVEN

```

## CURRENT

```

C          VALUE FOR A SPECIFIC RELAY
*****
SUBROUTINE RELAY(NDEV,CURR,TVAL,TDSET,DEV)
DIMENSION DEV(20,0/4)
TVAL=0.0
X=ALOG10(CURR)
IF(X.GT.1.2)X=1.2
DO 10 I=0,4
TVAL=TVAL+DEV(NDEV,I)*(X**I)
10 CONTINUE
IF(NDEV.EQ.7)TVAL=TVAL-2.0
TVAL=TVAL+TDSET
RETURN
END

```

```

*****
C          TITLE:LOG.LOG,MAKES LOG LOG FORM FOR GRAPH OF RELAY
CURVES
*****
C          OUTLINE BORDER
*****
C          MUST USE ALOG.LOG,@SYS:GRALIB
*****

```

```

SUBROUTINE LOG(IAOFF)
CALL ERASE
CALL MOVEA(0.0,0.0)
CALL DRAWA(0.0,750.0)
CALL DRAWA(1000.0,750.0)
CALL DRAWA(1000.0,0.0)
CALL DRAWA(0.0,0.0)
CALL MOVEA(900.0,5.0)
CALL DRAWA(900.0,750.0)
DO 200 N=0,4
DO 100 M=1,10
DN=10**N
XM=M*DN
IF(XM.GT.35000) GO TO 225
XX=(ALOG10(XM))*180
XTT=900-XX
CALL MOVEA(XTT,175.0)
CALL DRAWR(0.0,575.0)
100 CONTINUE
200 CONTINUE
225 CALL MOVEA(900.0,175.0)
CALL DRAWA(0.0,175.0)
DO 400 N=0,2
DO 300 M=1,10
DN=10**N
XM=M*DN

```

```

XX=(ALOG10(XM))*190
XT=XX+175
CALL MOVEA(95.0,XT)
CALL DRAWR(805.0,0.0)
300 CONTINUE
400 CONTINUE
DO 460 M=0,3
XN=175+190*M
CALL MOVEA(900.0,XN)
CALL NUMBER(10,'12')
CALL MOVER(0.0,10.0)
J=1A0FF+M
CALL NUMBER(J,'11')
460 CONTINUE
CALL CHRROT(90)
CALL MOVEA(960.0,400.0)
CALL ANCHOS('CURRE',5)
CALL ANCHOS('NT I',4)
CALL ANCHOS('N AMP',5)
CALL ANCHOS('S',1)
CALL MOVEA(900.0,0.0)
CALL DRAWA(900.0,750.0)
DO 500 M=0,5
XN=900-180*M
CALL MOVEA(XN,150.0)
IF(M.EQ.0)CALL NUMBER(.01,'F3.2')
IF(M.EQ.1)CALL NUMBER(.1,'F2.1')
IF(M.EQ.2)CALL NUMBER(1,'11')
IF(M.EQ.3)CALL NUMBER(10,'12')
IF(M.EQ.4)CALL NUMBER(100,'13')
IF(M.EQ.5)GO TO 510
500 CONTINUE
510 CALL MOVEA(20.0,140.0)
CALL NUMBER(1000,'14')
CALL CHRROT(0)
CALL MOVEA(200.0,755.0)
CALL ANCHOS('TIME ',5)
CALL ANCHOS('IN SE',5)
CALL ANCHOS('CONDS',5)
CALL MOVEA(0.0,0.0)
RETURN
END
*****
C SUBROUTINE CKTBKR; COMPUTES TIME VALUE FOR A GIVEN
CURRENT VALUE
C
*****
SUBROUTINE CKTBKR(ID,MDEV,DVAL,OFFSET,TVAL,ANVAL)
CVAL=DVAL-OFFSET

```



```

      IF(ID.NE.1)GO TO 50
      CVAL=CVAL+.1122
      IF(CVAL.GT.AMVAL.AND.AMVAL.NE.0)GO TO 90
      IF(CVAL.LT.0)GO TO 80
      TVAL=5.76908+(-10.88261*(CVAL))+(23.65419*(CVAL**2))+
(-34.7922
      1*(CVAL**3))+(33.77472*(CVAL**4))+(-21.14536*(CVAL**5
)))+(6.4
      231778*(CVAL**6))
      TVAL=TVAL-2.0
      GO TO 100
50      CVAL=CVAL+.232
      IF(CVAL.LT.0)GO TO 80
      AMVAL=AMVAL+.075
      IF(CVAL.GT.AMVAL.AND.AMVAL.NE.0)GO TO 95
      TVAL=5.8596722+(-4.394335*CVAL)+(-.50690284*(CVAL**2)
)+(10.40
      12739*(CVAL**3))+(-17.064956*(CVAL**4))+(13.011543*(C
VAL**5))
      2+(-4.010724*(CVAL**6))
      TVAL=TVAL-2.0
      GO TO 100
80      TVAL=6.0
      GO TO 150
90      TVAL=-2.0
      GO TO 100
95      TVAL=ALOG10(.025)
100     CONTINUE
150     RETURN
      END

```

\*\*\*\*\*

**APPENDIX C**

**DISK-FILE FORMATS**

## Disk file RES.DAT

$a_0$  Double precision wire resistance coefficients

.

$a_6$  Double precision wire resistance coefficients

$a_0$  Double precision wire reactance coefficients

.

$a_6$  Double precision wire reactance coefficients

## Disk file TEST.DAT

element number/line bus/load bus/positive seq p.u. impedance/zero  
seq p.u. impedance/transformer neutral imp line bus/transformer neutral  
imp load bus

00000

## Load data

bus number/p.u. VA/per unit subtransient reactance

0000

## Disk file XFER.DAT

line bus/load bus/inrush/low withstand/high withstand/transformer size

## LCUR.DAT

line bus/load bus/current at line bus/current at load bus

## FCUR.DAT

fault bus/element number/3 phase fault/1 phase fault

## DEV.DAT

device number/ $a_0/a_1/a_2/a_3/a_4$

**ADEV.DAT**

element number/element bus numbers/device numbers/line bus element  
low pickup, high pickup/load bus element low pickup, high pickup/  
magnetic settings line, load/time dial setting line, load/CT ratios  
line,load/

**APPENDIX D****SAMPLE PROGRAM DATA INPUT**

Before beginning the program sequence, RES.DAT and DEV.DAT contain the proper coefficients listed in Table 8.5. All source programs have been loaded and saved. PLOTD.F4 uses subroutines contained in the PDP10 system files so it must be loaded using:

LOAD PLOTD.F4, @ SYS:GRALIB.

The first program is started with run INPUT. Underlined words and numbers are data input by the user. Words not underlined are prompts from the computer in the input sequence that follows.

Do you want to read from a KYBRD?  
 <CR> for input from TTY, 1 for read. . .  
<CR>

Enter the problem base in MVA  
1

Enter the problem base in KV  
15

Enter element data as follows: Bus ( ) to ( )  
 (Length)(Size)(Transformer impedance (P.U.))(Transformer size  
 in MVA)(Transformer High Voltage in KV)(Transformer low  
 voltage in KV)

1 2 3000 6 -(element with no transformer)

2 3 356 .001 .005 1 15 4.1 -(element with a transformer)

Input transformer ZN in P.U. refer to BUS

Side, (BUS 2) (BUS 3). . .  
.001 .005 .001 .005

(This is continued for each element until all elements of  
 the type in RES.DAT have been entered)

0 -(tells computer no more elements)

At this point if another wire type is to be used the  
 following procedure applies if not skip this section  
 and proceed to ①.

Input Bus 1 voltage. . .0  
 Data is accepted and a list follows

(Here the computer types all computed information on the elements entered so that they may be checked for error.)

Now enter the load data in the following manner;. . .  
 (Bus)(Load in KVA)(Pwr Factor). . .or. . .(Bus)(Load in HP)  
 (Pwr Factor). . .or. . .(Bus)(Load in Amps)(Pwr Factor)  
 What method will you use?. . .VA, HP, or Amps?

S -(writes element data computed to disk)

End of execution

(Load RES.DAT with the new wire type coefficients)

RUN INPUT

Do you want to read from a KYBRD?

<CR> for input from a TTY, 1 for read. . . .

1

Old data is entered ready for new line data

Enter element data as follows. . . (Program runs as in the first section)

①

Picking up the program from completion of element data, the data entry follows.

Input Bus 1 Voltage. . ..15000

Input Bus 2 Voltage. . ..15000

Input Bus 3 Voltage. . ..4100

.

Input Bus 8 Voltage. . ..440

Data is accepted and a list follows

(Computer types computed element data).

Number of buses is 8

Now enter the load data in the following manner;. . .

(Bus)(Load in KVA)(Pwr Factor). . .or. . .(Bus)(Load in HP)

(Pwr Factor). . .or. . .(Bus)(Load in Amps)(Pwr factor)

What method will you use? KVA, HP, or Amps?

HP

Enter. . .

4 800 .80

What method will you use?. . .KVA, HP, or Amps?

HP

8 500 .90

(This is continued until all loads are entered?)

What method will you use?. . .KVA, HP, or Amps?

S

End of Execution

RUN LDFLO

End of Execution

RUN ZBUS

Enter the zero sequence impedance for the loads at each bus. . .

```

8 .001 .005 -for each load where the zero sequence impedance
      : will not be assumed to equal the positive sequence
      : impedance
0 -tells the computer there are no more entries
Enter the mutually coupled elements in per unit in the following
format, TEST.DAT has the element numbers. . ., (Element) (Element)
(Zero Sequence Value)
2 3 0 .001 (The zero must be entered because the coupling is a
reactive value)
0 -(no more or no coupling)
End of execution
RUN FALT
Enter the fault impedance (Real) (Imaginary)
0 0
End of execution
RUN COORD
All load currents are ready, use device number list
Select device for the load at bus 4
4
:
:
Select the device for the load at Bus 8
3
Input temperature for ambient shift, 1 for less than
110 Deg C, 2 for 60 Deg C
<CR> for no shift. . .
<CR>
Does the device have a magnetic element?(0)Yes
0
Select device for Bus 6 protecting element feeding load at Bus 8
4
Select the Westinghouse Co. relay, refer to Table 1
Does the relay have an inst. element if yes 0
0
:
:
      (Until all backup devices have been set).
      Enter the device for the Bus 6 of element 5
4
Select the Westinghouse Co. relay, refer to Table 1
Does the relay have an inst. element if yes 0
0
:
:
      (Until all devices in the system have been set).
Device listing -(Here the computer lists the matrix ADEV)
End of execution
Run PLOTD
Devices have been set if you want to plot graph paper 0 if not
type 1
0

```



This will plot curves based on the lowest voltage in the system

Input the current offset for the graph, integer 1

Input element number

7

Finished?

1 -(no, 0 yes)

Devices have been set if you want to plot graph paper

0 if not type 1

1

Input element number

6

Finished?

0

End of execution.

If a device did not plot as desired its settings can be changed in ADEV.DAT.

END

FILMED

11-83

DTIC